

1 **Abstract**

2 **Introduction** Prosthetic ankle-foot devices incorporating a hydraulic articulation between the
3 pylon and prosthetic foot have been shown to be beneficial to the gait of more active individuals
4 with unilateral transtibial amputation (UTA). However, the functional benefits of using hydraulic
5 ankle-foot devices to less active individuals with UTA are yet to be determined. The aim of the
6 current study was to investigate the effects on gait performance of using a non-ESR foot with a
7 hydraulic attachment, compared to an identical, rigidly attached foot during overground walking
8 in less active individuals with UTA.

9 **Materials and Methods** Kinematic and kinetic data were recorded while five individuals with
10 UTA, deemed K2 activity level by their prescribing physician, performed two-minute walk tests
11 (2MWT) and ten overground gait trials, in two conditions; using a hydraulically articulating ankle
12 foot device (HYD) and using a rigidly attached ankle foot device (RIG).

13 **Results** Walking speed during the 2MWT was increased by 6.5% on average, in the HYD (1.07
14 m/s) condition, compared to the RIG (1.01 m/s) condition (Cohen's $d = 0.4$). Participants displayed
15 more symmetrical inter-limb loading ($d = 0.8$), increased minimum forward centre of pressure
16 velocity ($d = 0.8$), increased peak shank rotational velocity ($d = 1.0$) and decreased prosthetic
17 energy efficiency ($d = 0.7$) when using the HYD compared to RIG device.

18 **Conclusions** Individuals with lower activity levels walk faster and therefore further when, using a
19 foot with a hydraulically articulating attachment, in comparison to a rigid attachment. A reduced
20 braking effect in early stance phase, as a result of the action of the hydraulic component present in
21 the articulating attachment, partially explains the improvement in walking performance.

22 **Keywords** Lower-limb amputation, Prosthetics, Foot device, Ankle, hydraulic.

23

24

25 **Introduction**

26 Prosthetic ankle-foot devices that incorporate hydraulically damped articulation between
27 the pylon and prosthetic foot are a relatively new development in prosthetic technology, having
28 only been widely commercially available for approximately ten years. Feet such as the Kinterra
29 (Freedom Innovations, Morgan, CA), Echelon (Chas. A Blatchford & Sons, Basingstoke, UK) and
30 MotionFoot (Fillauer, Chattanooga, TN) combine a hydraulic articulation unit with an energy
31 storing and returning (ESR) foot, and are primarily intended for use by individuals with higher
32 levels of mobility, such as those classified as being at least K3 on the Medicare Scale. The
33 hydraulic dashpots present in the articulation mechanism of such prosthetic ankle-foot devices
34 cause the ankle-foot system to absorb more and return less energy during stance than an identical,
35 rigidly attached, foot [1]. In addition, due to the hydraulic component, such ankle-foot devices also
36 weigh more than comparable, rigidly attached, feet.

37

38 Despite these apparent drawbacks, it has been reported that hydraulic ankle-foot devices
39 provide functional benefits during walking, when compared to feet that are either attached without
40 articulation, or attached via an elastic articulation device. The primary reported functional benefit,
41 when using a hydraulic ankle-foot device, in more active (K3) individuals with lower limb
42 amputation, is an increase in the individual's walking speed [1-4]. Walking speed is a primary
43 measure of gait function in individuals with lower-limb amputation [5]. Furthermore, for
44 individuals with a lower-limb amputation, an increase in walking speed reflects improved gait
45 function during and following rehabilitation [6-8], and is also associated with decreased temporal
46 asymmetry [9]. This increase in walking speed, when using a hydraulic ankle-foot device, appears

47 to be driven by a reduction in inappropriate fluctuations of centre of pressure progression during
48 prosthetic-limb stance [2], where the centre of pressure becomes stationary or travels backwards
49 beneath the prosthetic hind and/or mid foot [10,11]. In addition to this, hydraulic articulation has
50 been found to result in increased forwards angular velocity of the prosthetic shank during early
51 stance [2]. These effects occur despite the devices' hydraulic dashpots dissipating energy during
52 stance, resulting in reduced energetic efficiency compared to that of a rigidly attached foot [1].
53 Accordingly, the increased walking speed appears to be due to a reduced 'braking effect' [12],
54 rather than increased propulsion, allowing the transfer of weight onto the prosthetic limb to occur
55 more smoothly [2]. Another effect of using a hydraulic ankle-foot device is a reduction in load-
56 bearing asymmetry during walking [1], that possibly contributes to a reported reduction in in-
57 socket pressures, due to reduced loading rates [13]

58

59 The effects of using a hydraulic ankle-foot device have been observed in individuals with
60 both unilateral transtibial (UTA) and transfemoral amputation [14] although, again, only in
61 patients who are described as being at least K3 on the Medicare Mobility Scale. Individuals who
62 are less mobile are seldom prescribed ESR feet, and therefore, rarely use feet with hydraulic
63 'ankle' function. However, the apparent benefits of using hydraulic ankle-foot devices observed
64 in more mobile individuals may also occur in the less active. This suggestion is supported by a
65 low-activity group self-reporting improvements in their gait and prosthesis satisfaction when their
66 prosthetic prescription was changed to include a hydraulic ankle-foot device [15].

67

68 Therefore, the aim of this study was to investigate the effects, of using a non-ESR foot with
69 a hydraulic attachment, during overground walking, compared to an identical, rigidly attached

70 foot, in individuals with UTA, described as being K2 on the Medicare scale. It was hypothesized
71 that, (1) when using the hydraulic ankle-foot device, individuals would walk faster compared to
72 when using an identical, rigidly attached foot device. It was expected that any increase in walking
73 speed would be due to the same drivers previously reported in more active individuals when using
74 a prosthetic ankle-foot device that incorporates a hydraulically articulating attachment. Thus, it
75 was also hypothesized that, (2) there would be an increased minimum forwards/peak backwards
76 velocity of centre of pressure progression beneath the prosthetic foot, increased angular velocity
77 of the prosthetic shank during early stance and a reduction in stance phase load bearing asymmetry
78 between the intact and residual limbs when using the hydraulic compared to rigidly attached ankle-
79 foot device. Finally, it was expected that these effects would occur despite a reduction in efficiency
80 of the ankle-foot device, due to the hydraulic unit dissipating energy during stance.

81

82 **Methods**

83 *Participants*

84 Five individuals with UTA, currently assessed as being K2 on the Medicare scale by their
85 prescribing physician, were recruited from the same prosthetic limb and rehabilitation centre. All
86 provided written informed consent prior to participation in the study, which was approved by the
87 Nottingham Trent University Human Research Ethics Committee (Table 1).

88

89 ***Insert Table 1 here***

90

91 Participants were recruited and included, if they: 1) were community living adults aged between
92 18 and 65 years of age; 2) were able to walk without walking aids for periods of at least two

93 minutes; 3) partook in physical activity at least once a week for 30 minutes; 4) had good (corrected,
94 if necessary) vision and 5) had no unresolved health issues, as determined using a health screening
95 questionnaire. Individuals were excluded, if they: 1) had experienced an unintentional fall in the
96 previous 12 months; 2) experienced undue pain while walking; 3) were current smokers or 4) were
97 currently taking five or more prescribed medications.

98

99 *Experimental Design*

100 Participants were required to complete the below described walking tasks while using the
101 same habitual socket/liner and same non-ESR foot, attached under two different conditions: (1)
102 using a hydraulically articulating attachment (HYD - Avalon^{K2}) and (2) using a rigid non-
103 articulating attachment (RIG - Navigator; both Chas A. Blatchford & Sons, Basingstoke, UK;
104 Figure 1). These feet were chosen as they are identical, save for the nature of attachment to the
105 prosthetic pylon. In order to ameliorate any order effects, the order in which participants completed
106 walking tasks were counterbalanced across participants according to which was their habitual
107 device, regardless of whether this was the RIG or HYD. For each condition participants initially,
108 completed a familiarisation trial followed by a measured trial of the two-minute walk test (2MWT).
109 The 2MWT comprised two 15m straight sections with a 180 degree turn at either end, in order to
110 mitigate the effects of turning on walking test performance [16] [17]. Participants then completed
111 10 discrete overground walking trials along a 15m instrumented walkway including two force
112 plates. Participants were instructed for all tests to walk as they would normally. The same highly
113 experienced prosthetist made all necessary adjustments to all participants' prostheses, when
114 changing between prosthetic conditions. Other than different ankle-foot device attachment, there
115 was no difference in the prostheses between conditions. Participants were asked to complete the

116 Activities-specific Balance Confidence Scale (ABC) [18], the Houghton Scale of Prosthetic Use
117 (Houghton) [19] and the Prosthetic Limb Users Survey of Mobility (Plus-M 12) [20] which are
118 self-report questionnaires providing information on participants self-perception of balance
119 confidence, prosthetic use and mobility, respectively. Higher scores on these scales reflect
120 increased balance confidence (ABC), prosthesis use (Houghton) and mobility (Plus-M 12).

121 ***Insert Figure 1 here***

122

123 *Experimental Protocol*

124 Participants attended data collection sessions wearing comfortable clothing and their
125 normal everyday shoes. In order to define a seven segment model of the lower limbs (feet, thighs,
126 shanks) and pelvis, reflective markers (14 mm diameter) were affixed bilaterally to participants at
127 the following locations: 1st and 5th distal metatarsal heads, lateral border and anterior aspect of
128 the foot, calcaneus, medial and lateral malleoli and femoral epicondyles and anterior and posterior
129 superior iliac spines. A rigid cluster of four markers was also affixed to the lateral side of each
130 shank segment. Foot markers were placed over the shoes. Marker placement on the
131 residual/prosthetic limb was estimated from anatomical landmarks on the intact limb [6] with the
132 prosthesis being modelled as a unified deformable segment [21]. Participants commenced each
133 2MWT trial by standing at the end of the walkway and were free to self-select a turning direction.
134 The number of strides taken by each participant during the 2MWT were recorded by an
135 investigator using a hand tally counter and the two-minute walk distance (2MWD) was recorded.
136 Participants then completed the overground walking trials at a self-selected speed, for which start
137 positions were adjusted to ensure a clean contact with the forces platforms without any obvious
138 targeting or adjustment to stride pattern. A nine-camera motion capture system (Oqus 400,

139 Qualisys AB, Gothenburg, SE) and two force plates (OR6-7, AMTI, Watertown, MA, US)
140 recorded kinematic and kinetic data at 100Hz and 500Hz, respectively. A static calibration was
141 performed by collecting kinematic data of each participant standing in the anatomical position.
142 Participants were afforded rest breaks as and when required.

143

144 *Data Analysis*

145 Each 2MWT trials yielded outcome measures of two-minute walk distance (2MWD),
146 walking speed (m/s), determined by dividing the recorded 2MWD by 120 seconds, and the number
147 of strides (stride count). To obtain other variables, biomechanical data for the 10 overground
148 walking trials were analysed. The raw kinematic data were interpolated using a cubic spline
149 algorithm and both the kinematic and kinetic data were smoothed using a zero-lag Butterworth
150 filter with a 6 Hz cut-off frequency (Visual3D, C-Motion, Germantown, USA). Heel strike and toe
151 off were defined as ascending and descending thresholds of 20 N in the vertical component of the
152 ground reaction force, respectively. The following biomechanical outcome measures were
153 calculated: 1) Load bearing symmetry; defined as the ratio of the peak vertical component of the
154 ground reaction force during intact and prosthetic limb stance, 2) peak shank rotational velocity;
155 defined as the peak angular velocity of the prosthetic shank in the sagittal plane from prosthetic
156 heel strike until intact toe off, 3) minimum centre of pressure (COP) velocity; defined as the
157 minimum forwards or peak backwards (in the direction of travel) velocity of the COP during
158 prosthetic limb stance, and 4) prosthetic energetic efficiency; defined as the ratio of energy
159 absorbed and energy returned by the prosthetic foot device during prosthetic limb stance. Energy
160 absorbed and returned were defined as the positive and negative integrals, respectively, of unified
161 deformable segment power during prosthetic limb stance [21]. For each participant, the outcome

162 variables were calculated for each trial, in each prosthetic condition, and the mean for each
163 condition was computed using the results from each trial. No inferential statistical analyses were
164 made, rather, the results for each participant, in each prosthetic condition are presented. This
165 approach was taken due to participants' reaction to altered prosthetic componentry being an
166 individual response [4] and the small group size. Effect sizes (Cohen's d) were calculated using
167 group mean and standard deviation differences between prosthetic conditions [22]. An effect size
168 ≥ 0.4 was operationally defined as being clinically meaningful in the current study [23].

169

170 **Results**

171 *Two-minute walk test outcome measures*

172 During the 2MWT, participants walked, on average, with a 6.5% increase in self-selected
173 walking speed ($d = 0.4$, Figure 2), and thus an increased 2MWD ($d = 0.4$, Table 2), when using
174 the HYD compared to the RIG device. This increase in walking speed and 2MWD using the HYD
175 device was present across all participants. The number of strides taken during the 2MWT also
176 increased using the HYD, when compared to the RIG device in all participants, although not to the
177 same extent as the walking speed, with, on average, a 3.9% increase ($d = 0.3$, Table 2).

178

179 ***Insert Figure 2 here***

180 ***Insert Table 2 here***

181

182 *Biomechanical outcome measures*

183 All participants' load bearing was more symmetrical between limbs ($d = 0.8$, Table 3) when
184 using the HYD compared to RIG device. Similarly, peak shank rotational velocity ($d = 1.0$, Table

185 3) increased for all participants except one, and minimum forward COP velocity ($d = 0.8$, Table
186 3) increased for all, when using the HYD compared to RIG device. The HYD device tended to
187 absorb more, and return less, energy during stance phase, which resulted in a reduced prosthetic
188 energy efficiency for all participants, when using the HYD device compared to the RIG device (d
189 $= 0.7$, Table 3).

190

191 **Discussion**

192 The aim of the current study was to investigate the effects of using a hydraulically
193 articulating ‘ankle’ attachment versus a rigid non-articulating attachment with a non-ESR
194 prosthetic foot, on gait performance during level gait in individuals with UTA, described as being
195 K2 on the Medicare scale by their physician. The first hypothesis, that when using the hydraulic
196 ankle-foot device, individuals would walk faster compared to when using an identical, rigidly
197 attached foot device, was supported. Every participant in the current study walked more quickly,
198 and thus on average 7.8m further, during the 2MWT when using the hydraulic ankle-foot device
199 compared to when using the rigidly attached foot. Additionally, post-hoc analysis indicated that
200 during the 10 discrete trials, participants mean (SD) walking speed was greater using the hydraulic
201 ankle-foot device compared to using the rigidly attached foot (HYD, 1.19 (0.09) m/s, RIG, 1.16
202 (0.10) m/s). In addition, walking speed was greater in both prosthetic conditions during discrete
203 trials compared to during the 2MWT. This observation of increased walking speeds during discrete
204 trials vs. continuous walking in the current study are consistent with previous reports from healthy
205 individuals [24]. Increases in walking speed have been previously demonstrated in individuals
206 with UTA with higher levels of physical function [1-4]. One cohort study of more active
207 individuals [2] reported a 7% increase ($d = 0.5$) in self-selected walking speed when using a

208 hydraulic ‘ankle’ device, which is similar to the results of the current study (6.5% increase, $d =$
209 0.4). Thus, we feel that, despite the current study being a case-series rather than cohort study, it
210 demonstrates that hydraulic ‘ankle’ function also appears to benefit those defined as having a
211 relatively low level of activity.

212

213 Increased walking speed is positively correlated with improved self-efficacy of gait among
214 individuals with lower-limb amputation [25]. Every participant in the current study walked more
215 quickly with the HYD and stated a preference for using the HYD rather than the RIG device. This
216 preference corroborated a previous report of improved user satisfaction when using an Avalon^{K2}
217 ankle-foot device [15]. Following data collection, all were offered whichever ankle-foot device
218 (HYD or RIG) they preferred (if it was not their currently prescribed device), to be provided to
219 their prosthetist for subsequent fitting. Four of the five participants, whose currently prescribed
220 device was the RIG, opted for the HYD. The fifth participant, who used a HYD prior to data
221 collection, retained that device. Anecdotal, but interesting nonetheless, following data collection
222 all participants were asked whether they had felt as if they were walking faster when using one
223 ankle-foot device in particular and all said no. It is well documented that self-selected walking
224 speed is related to minimising energy expenditure (e.g. [26]). Although joint kinetics were not
225 outcome variables in the current study, previously it has been reported that use of a similar HYD,
226 but with an ESR foot, resulted in a reduction in mechanical work per metre travelled at the intact
227 limb in more active individuals [2], which possibly contributed to a significant reduction in
228 metabolic cost due to the function of the HYD [14]. Although no supporting data is presented from
229 the current study it may be postulated that, given the increase in walking speed and lack of

230 awareness of such among participants, use of a HYD device has similar effects in less mobile
231 individuals too. This suggestion should certainly be the subject of future research.

232

233 The second hypothesis related to the biomechanical explanation of the predicted increased
234 walking speed associated with the hydraulically articulating ankle-foot device. The hypothesis that
235 there would be an increased minimum forwards/peak backwards COP velocity beneath the
236 prosthetic foot, increased angular velocity of the prosthetic shank during early stance and a
237 reduction in stance phase inter-limb load bearing asymmetry was supported in the majority of
238 participants. These findings were consistent with those previously reported in higher activity
239 individuals with the same level of amputation walking using devices with similar functions [1,2]
240 and go some way in explaining the increases in walking speed observed in the current study. The
241 increased energy absorbed and dissipated, rather than returned, by the hydraulic dashpot present
242 in the HYD may have allowed the individuals to load the residual limb to a greater extent. This
243 was reflected in the increase in inter-limb loading symmetry, without the requirement for this
244 energy to be attenuated by deformation in the remaining proximal biological joints and/or
245 structures e.g. biological knee joint, residuum-socket interface. There are no supporting data, thus
246 it is speculation, but this could be the driver of reduced in-socket pressures reported when using a
247 hydraulic ankle-foot device [13]. In addition, the improved forward COP progression and shank
248 angular velocity (that was displayed in all participants except P1) when using the hydraulic ankle-
249 foot device, reflected smoother centre of mass progression during prosthetic stance. The increase
250 in minimum forward COP velocity in all participants (including P2, though remaining marginally
251 negative) also reflected a reduction in the ‘dead spot’ reported by some individuals with lower
252 limb amputation, as progression over the prosthetic limb is interrupted during stance phase. When

253 considered together, these factors point to an overall reduced ‘braking effect’ [12], particularly
254 during early stance, when using the hydraulic ankle-foot device. It would seem that shifting the
255 functional requirements from the biological structures to the mechanical device during early stance
256 is potentially beneficial, where individuals exchange the static stability of the non-articulating rigid
257 ankle-foot device for the dynamic ability of the hydraulically articulating ankle-foot device. Future
258 research should attempt to investigate whether similar effects are observed in the same patient
259 group when performing other, commonly encountered activities of daily living such as stepping,
260 stair ascent/descent and walking on slopes and uneven surfaces.

261

262 There were only five participants in the current study, however research has shown that
263 reactions to a change of prosthetic device are specific to the individual [4]. Often within a cohort
264 study, a significant group effect is observed between conditions, while some individuals within
265 the group display no, or the opposite reaction. The increased walking speed, when using the HYD,
266 was present for all participants. Likewise, the biomechanical differences that occurred between
267 device conditions were consistent, and almost ubiquitous, across participants. Only one individual
268 did not present increased angular velocity of the prosthetic shank when using the HYD. All others
269 responded as hypothesised across all outcome variables. Therefore, despite the small sample size,
270 we feel that the findings from the current study are of clinical relevance at both the individual level
271 and also to national health care providers. The demonstrated increases in walking speed suggest
272 that improved mobility in an individual may be achieved via prescription. This increased mobility
273 could possibly lead to subsequent improved completion of daily tasks and/or engagement in social
274 activities. In addition, given that patients themselves previously reported a perceived benefit of
275 such devices to mobility and prosthetic satisfaction [15], this could suggest that widespread use of

276 such devices may be beneficial to the wider body of less active individuals living with unilateral
277 transtibial amputation. However, prior to the widespread adoption of such devices, the long-term
278 effects and potential benefits to both the individual and healthcare systems of such hydraulically
279 articulating ankle-foot devices must be established and should be the focus of future investigation.

280 ***Limitations***

281 There are a number of limitations to the current study, the most obvious of which is the
282 size of the sample, which was limited to include only individuals who used the specified
283 components in order to prevent any differences being due to the foot, itself, rather than the change
284 in attachment. Although the sample size was only five individuals, prosthetic prescription is made
285 on an individual basis. For every participant in the current study, large and consistent effects were
286 observed, thus authors feel that the presented results are still valid. Authors do, however,
287 acknowledge that confirmatory future research should attempt to assess whether these magnitudes
288 of effect are maintained in the wider patient population. Also, the effects observed in the current
289 study were acute (same day) and do not speak to any long-term effects. This begs the question as
290 to whether these difference would be maintained over longer periods of time and what the
291 subsequent influences would be on physical activity and quality of life. This not answerable by the
292 current study but warrants further investigation. Finally, a highly experienced prosthetist with
293 knowledge of all of the components, made all adjustments in the current study. However, where
294 this is not possible, it remains to be seen if similar effects would be observed.

295

296 **Conclusion**

297 Individuals with unilateral transtibial amputation who are described as K2 by their
298 prescribing physician walk faster when using a non ESR-foot with a hydraulically articulating

299 attachment when compared to an identical foot with a rigid, non-articulating attachment. This
300 improvement in walking performance can be partially explained by a reduced ‘braking effect’ in
301 early stance as a result of the action of the hydraulic component present in the articulating
302 attachment.

303

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309

310 **Declaration of Interest**

311 The authors report no conflicts of interest. The authors alone are responsible for the content
312 and writing of the paper.

313

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