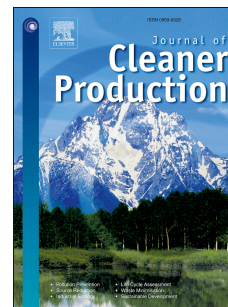


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Achieve clean and efficient biomethane production by matching between digestate recirculation and straw-to-manure feeding ratios

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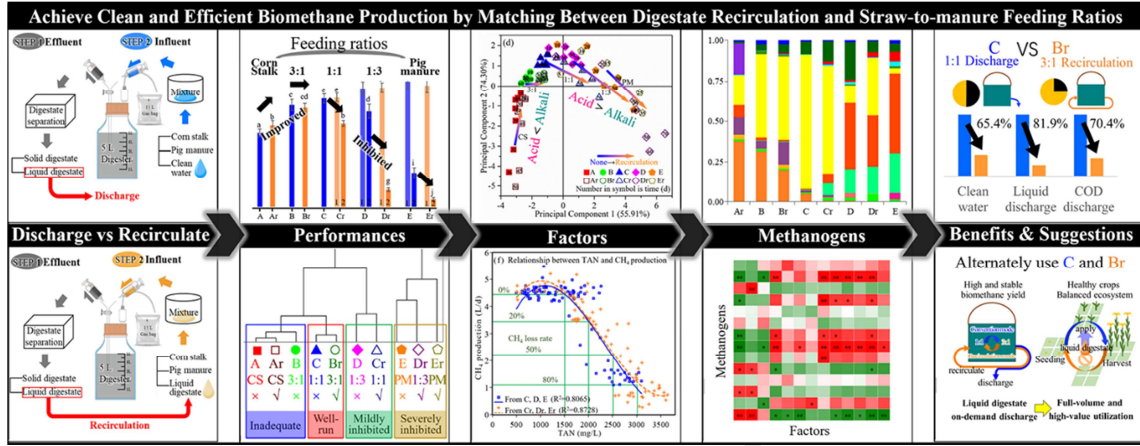
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1 *There are 7671 words, including whole text file, tables, and figure captions.*

2 **Abstract**

3 Liquid digestate recirculation can fundamentally solve the problem of voluminous liquid
4 digestate discharge for biogas projects. However, the uncertainty of the effect of
5 recirculation under different feedstock restricts the application of recirculation
6 technology. In this study, the comprehensive effects of straw to manure feeding ratios
7 and liquid digestate recirculation on anaerobic digestion performance and microbial
8 community structure were investigated. Recirculation was beneficial for biomethane
9 production and digestion stability in digesters of corn stalk and straw/manure 3:1 by
10 alleviating the loss of ammonia and alkalinity, while it aggravated the accumulation of
11 ammonia and organic acids and reduced methane yield under 1:1, 1:3 and pig manure.
12 The feeding ratios and recirculation formed a combined effect on ammonia
13 concentration in the fermentation system, and when the total ammonia concentration
14 was above 1,500 mg/L, acids accumulation and decline in methane production would
15 occur whether with recirculation or not. The microbial community structure varied
16 corresponding to the fermentation state. In the well-run digesters, which were 3:1 with
17 recirculation and 1:1 without recirculation, the dominant methanogens were
18 Methanosaeta, while in the inhibited digesters, Methanosarcina and Methanosphaera
19 dominated the methanogen community. Based on producing 1 GJ energy, the strategy of
20 3:1 with recirculation reduced the discharge of liquid digestate by 81.9 % and the use of
21 clean water by 65.4 % compared to that of 1:1 without recirculation. An integrated

22 approach of adjusting feedstock formula and selectively employing liquid digestate
23 recirculation was proposed to produce liquid digestate on-demand with downstream
24 application requirement, which will make biogas industry eco-friendly and
25 cost-effective.

26 **Keywords**

27 Anaerobic co-digestion; Digestate recirculation; Straw-to-manure ratio; Corn stalk; Pig
28 manure.

29 **1 Introduction**

30 Anaerobic digestion is the most commonly used route to deal with much
31 agricultural waste, providing useable and renewable energy in the form of biogas
32 (Frigon and Guiot, 2010; Ward et al., 2008). Biogas production from agricultural waste
33 will help offset fossil fuel demand, reduce pollution from agricultural waste and fossil
34 fuel consumption (Patrizio et al., 2015), and also upgrade matter cycling in agricultural
35 sectors to produce high-quality food and other products (Alburquerque et al., 2012).

36 Digestate, also known as effluent or residues, is the byproduct of anaerobic
37 digestion, and the disposal of which is the basis for the continuous operation of biogas
38 projects (Monlau et al., 2015). With the increase and expansion of biogas projects, the
39 amount of digestate simultaneous increase. The eco-friendly and low-cost disposal of
40 excessive digestate, especially the liquid part, has become an urgent problem hindering
41 the promotion of anaerobic digestion technology (Gong et al., 2013; Hu et al., 2014).
42 Irrigation is a common practice of liquid digestate (Tambone et al., 2017). However, in

43 China, due to the lack of transportation facilities, the liquid digestate can only be poured
44 into the surrounding farmland. More importantly, the positive effect of applying liquid
45 digestate in farmland needs to be based on the demand for crop fertigation, which is
46 seasonal and intermittent. The continuous discharge tends to cause the soil to exceed its
47 bearing capacity and cause serious pollution (Rehl and Muller, 2011). In some European
48 countries, liquid digestate needs to be stored for more than 180 days before irrigation,
49 which occupies a huge space and also emits pollutants (Xia and Murphy, 2016). Seeking
50 alternative approaches to reuse liquid digestate is a global requirement for the economy
51 and sustainability of most biogas projects.

52 An alternative approach to reduce the volume of effluent is to recirculate liquid
53 digestate back into digesters (Jarvis et al., 1995; Nie et al., 2015; Zuo et al., 2015). Other
54 than discharge reduction, liquid digestate recirculation can also reduce the overall water
55 consumption of biogas projects, which cuts costs and also saves water resources. And
56 the overall energy consumption can also be reduced through recirculation due to the
57 recovery of retained heat in warm liquid digestate (Wang et al., 2018). However, whilst
58 recirculation can improve fermentation efficiency (Peng et al., 2016) and system
59 stability (Gottardo et al., 2017) by recycling nutrients, buffers and microorganisms (Li et
60 al., 2018; Ratanatamskul and Saleart, 2016), it can also result in the accumulation of
61 fermentation inhibitors (Estevez et al., 2014) and non-degradable substances (Ni et al.,
62 2017) leading to inefficient digestion and even process failure (Wu et al., 2016;
63 Zamanzadeh et al., 2016). Previous studies have focused on the effect of liquid digestate

64 recirculation under particular one feedstock and/or process. However, the effect of liquid
65 digestate recirculation under different feedstock formula has not been compared. And
66 how liquid digestate recirculation affects the co-digesting system and microbial
67 community structure of crop straw and livestock manure has not been reported.
68 Considering the diversity of feedstock characteristics and many co-digestion situations,
69 studies on the interaction between feedstock ratios and the effect of recirculation will
70 help give full play to beneficial parts of recirculation impacts and avoid the adverse
71 effect.

72 The aim of this study is to investigate the effect of liquid digestate recirculation
73 under different ratios of crop straw and livestock manure on semi-continuous anaerobic
74 digestion. Corn stalk (CS) and pig manure (PM) were taken as representatives of crop
75 straw and livestock manure since they make up the larger proportion of their types.
76 Systematic data (gas production and fermentation characteristics) was obtained and
77 discussed from ten lab-scaled digesters semi-continuously fed by five feedstock ratios
78 with or without liquid digestate recirculation. Bacterial and Archaeal community
79 structure was investigated by high-throughput sequencing. Emission and consumption
80 per unit energy output were compared between well-performed digesters without and
81 with recirculation. The appropriate feedstock ratios and the suggestion for feedstock
82 adjustment were provided to take advantage of recirculation. The benefits of liquid
83 digestate recirculation were quantified. Results of this study indicated that, by
84 appropriately adjusting the feedstock and fermentation parameters, liquid digestate

85 recirculation could be successfully applied to most biogas plants playing the role of
86 reducing waste and recycling matter, water, and energy, which will make biomethane
87 production cleaner and more efficient.

88 **2 Material and methods**

89 Source, characteristic, and preparation of feedstock and inoculum were detailed
90 presented in 2.1. Design, operation and sampling of anaerobic digestion were
91 introduced in 2.2. Methods were classified by analyzing gas, digestate, and
92 microorganisms, and were listed in 2.3. Tools used in data analysis and graphical
93 presentation were summarized in 2.4

94 **2.1 Feedstock and inoculum**

95 Corn stalk (CS) was collected from the Shangzhuang Experimental Station (Beijing,
96 China) of the China Agricultural University, milled with a high-speed pulverizer
97 (FW100, Taisite, Tianjin, China), and stored at room temperature. Pig manure (PM) was
98 collected from a pig farm (Hebei, China) of the China Agricultural University. PM was
99 stored at room temperature in sealed barrels and mixed evenly before daily feeding of
100 the digesters. The inoculum was collected from a 65-L constantly-run continuous stirred
101 tank reactor in Lab of West Campus, Center of Biomass engineering, China Agricultural
102 University. The CSTR was fed by rice straw and dairy manure and run at 37 °C with an
103 average daily methane yield of 90 L/d for over two months. About 5 L effluent of the
104 CSTR was collected every day and stored in a 50-L sealed barrel at room temperature
105 until the barrel was full. Then, the collected effluent was stored anaerobically at 37 °C

106 for two months, and was thoroughly stirred once a day to eliminate the interference of
107 residual substrates in methane yield and to form homogenous inoculum. The
108 compositions of CS, PM, and inoculum are presented in Table 1.

109 2.2 Experimental design

110 To simulate different feedstock conditions, the following five recipes were selected
111 as follows: only CS, 3:1, 1:1, 1:3, and only PM, the proportions of which (CS:PM) were
112 based on their volatile solid (VS) contents. In each case, experiments were carried out to
113 compare performance with and without recirculation of the liquid digestate. The
114 experimental design is summarized in Table 2. Treatments without recirculation were
115 labeled A to E; treatments with recirculation were labeled Ar to Er. Digestion was
116 carried out in ten digesters, each with a total volume of 6.2 L, and a working volume of
117 5.0 L. Digestions were carried out under mesophilic conditions (37 °C), and were fed
118 once a day. The organic loading rate (OLR) was 4.0 g-VS/(L·d) and both the hydraulic
119 retention time (HRT) and the solid retention times (SRT) were 20 d. Digestions were
120 initiated by the addition of 5.0 L of inoculum and then discharged 250 mL digestate and
121 injected 250 mL feedstock every day. For digesters with recirculation, the discharged
122 250 mL digestate was liquid-solid separated by centrifuging 5 min at 3,000 rpm (CR3i,
123 Thermo Electron Co., Waltham, MA, USA), after which, 150 mL of the liquid digestate
124 was recirculated to digester by replacing 150 mL water in preparation of feedstock. The
125 biogas generated by each digester was collected in a 15-L gas bag. The compositions
126 and volumes of biogas produced by each digester were measured daily. Approximately

127 20 mL of effluent from each digester was sampled every other day and frozen at -35 °C
128 prior to further analysis.

129 2.3 Analytical methods

130 Biogas: volumes were monitored using the water displacement method and then
131 converted to a volume at standard conditions (0°C, 101.325 kPa). Methane content was
132 analyzed using a biogas analyzer (GA5000, Geotech, Britain).

133 Digestates: total solid (TS) and volatile solids (VS) contents, alkalinity, total carbon,
134 and total nitrogen were analyzed using standard methods (APHA, 2017). The pH was
135 determined using a pH meter (SX610, Sanxi, China). Cellulose and hemicellulose
136 contents were analyzed using a fiber analyzer system (Ankom 2000, Ankom Technology
137 Corp., Fairport, NY, USA). Concentrations of lactic acid and volatile fatty acids (VFAs)
138 including formic, acetic, propionic and butyric acids were analyzed using a high
139 performance liquid chromatography (HPLC) system equipped with an ion-exchange
140 column (Aminex HPX-87H; 300 mm x 7.8 mm, BioRad Laboratories, Hercules, CA,
141 USA) and a diode array detector (SPD-M20A, Shimadzu, Kyoto, Japan). Samples were
142 centrifuged at 12,000 rpm for 30 min (CR3i, Thermo Electron Co., Waltham, MA, USA),
143 and the supernatants were filtered through a 0.22 µm filter (Nylon66, Jinteng
144 Experimental Equipment Co., Ltd., Tianjin, China). Dilute sulfuric acid (5 mmol/L) was
145 applied as the eluent (0.6 mL/min) at 35°C (Cai et al., 2018). The concentration of total
146 ammonia nitrogen (TAN) was measured by a flow injection analyzer (AA3, SEAL,
147 Germany). The concentration of the free ammonia nitrogen (FAN) was calculated based

148 on equation Eq. (1) (Hansen et al., 1998).

$$149 \quad [FAN] = [TAN] \times \left(1 + \frac{10^{-pH}}{10^{-(0.09018 + \frac{2729.92}{T(K)})}} \right)^{-1} \quad \text{Eq. (1)}$$

150 Where [TAN] is the concentration of total ammonia (mg/L), [FAN] is the
151 concentration of free ammonia (mg/L), and T(K) is the temperature (kelvin).

152 Microbial analysis: total microbial DNA was extracted from 3 mL of effluent from
153 digesters at the 60th day using a bead beating plus column purification (RBB + C) as
154 previously reported by Zhao et al. (2017). High-throughput (Illumina Miseq) sequencing
155 was conducted by Majorbio Co., Ltd. (Shanghai, China). PCR and Illumina Miseq
156 sequencing were conducted as described by Zhao et al. (2017). The primer sets 338F
157 and 806R (5'-ACTCC TACGGGAGGCAGCA-3' and
158 5'-GGACTACHVGGGTWTCTAAT-3') were used for bacteria, and primer sets
159 524F-10-extF and Arch958-modR (5'-TGYCAGCCGCCGCGGTAA-3' and
160 5'-YCCGGCGTTGAVTCCAATT-3') were used for archaea. The reads were assigned
161 operational taxonomic units (OTUs) at 97 % sequence similarity. Community structure
162 was analyzed at the phylum and genus levels using the Silva database (Release 115
163 <http://www.arb-silva.de>) (Zhao et al., 2017).

164 2.4 Statistical analysis

165 Statistical significance was evaluated by using univariate analysis of variances at a
166 P-value of less than 0.05 in IBM SPSS Statistics 25. Cluster analysis and principal
167 component analysis (PCA) were conducted using all measured parameters, including
168 methane production, pH, alkalinity, lactic acid, and volatile fatty acids. Origin 9.0 and

169 Canoco for Windows 4.5 was used for data analysis and graphical presentation.

170 **3 Results and discussion**

171 The responses of digester performance to liquid digestate recirculation under
172 varying straw/manure ratios were investigated. The interaction between feeding ratios
173 and recirculation was analyzed and discussed. Microbial communities in digesters of
174 different strategies, including feeding ratio and whether with recirculation, were
175 observed, and the relationship among operation strategies, fermentation parameters, and
176 microbial community was discussed. Finally, the benefits of proper use of recirculation
177 were quantified, and practical suggestions were drawn to guide the appropriate
178 application of recirculation by summarizing the optimized strategies.

179 3.1 Effects of feeding ratios and recirculation on digester performance

180 The effect of digestate recirculation under varying feeding ratios on digester
181 performance were discussed by promotion in section 3.1.1 and inhibition in section 3.1.2.
182 Performance enhancement by liquid digestate recirculation was observed in digesters
183 fed with only CS and CS:PM 3:1, and performance inhibition was observed in digesters
184 fed with CS:PM 1:1, 1:3, and only PM. The interaction of feeding ratios and digestate
185 recirculation was discussed in section 3.1.3.

186 3.1.1 Improved effects of recirculation under CS and CS:PM 3:1

187 The stable period of methane production, which was day 6-20 for A and day 6-35
188 for Ar, was prolonged 15 d with the recycled utilization of liquid digestate (Fig. 1a). The
189 methane production significantly ($P<0.05$) increased from 3.08 ± 0.16 L/d for A to $3.38\pm$

190 0.20 L/d for Ar with an increased efficiency of 10 %, showing the effect of liquid
191 digestate recirculation on methane production enhancement when fed with only CS..
192 The pH, alkalinity, and TAN of stable periods of both A and Ar decreased as digestion
193 proceeded, indicating that the buffer substances and nitrogen nutrients discharged along
194 with digestate were more than those added along with feedstock and produced by
195 digestion. The decline of pH, alkalinity, and TAN in Ar was slower than that of A,
196 because soluble matter in liquid digestate recycled back to digesters, which made a
197 decreased dilution of buffer substances and nitrogen nutrients. As a result, the stability
198 of digesters was improved by recirculation through reutilization of the buffer substances
199 and nitrogen nutrients, so the longer period of high process performance was achieved in
200 Ar than A. Consistent conclusions were draw in Li et al. (2018) and Peng et al. (2016),
201 where liquid digestate recirculation achieved methane production enhancement of 11 %
202 and 21 % along with stability improvement. When the pH decreased to under 6.8,
203 alkalinity decreased to under 2.0 g/L, and TAN decreased to under 50 mg/L (day 24 for
204 A and day 40 for Ar), total acids concentration sharply increased (Fig. 2a&b), showing
205 an imbalanced state of digesters. It is obvious that the supplementation of buffering
206 capacity by liquid digestate recirculation did not fill the loss of buffer substances
207 through discharge when fed by only CS, so Ar still failed at the end. Before the
208 concentration of acids increased, there was no significant difference ($P>0.05$) in the
209 concentration of total acids between A and Ar, all of which were 0.24 ± 0.01 g/L. Since
210 hydrolysis of crop straw is the key rate-limiting step in anaerobic digestion (Yu et al.,

211 2016), and acids (mainly substrates for methanogens) was in a deficiency in Ar, it was
212 inferred that the acids returned by recirculation was directly converted into methane and
213 formed the increase of methane production in Ar.

214 As in digesters fed with CS:PM of 3:1 without (B) and with (Br) liquid digestate
215 recirculation, gas production continued at a steady and high level for the duration of
216 experiment (Fig. 1b), and no significant difference ($P>0.05$) between B and Br was
217 observed on methane production and proportion. It is consistent with results obtained by
218 Hu et al. (2014), who investigated anaerobic digestion of CS added with urea ($C/N=25$)
219 with and without liquid digestate recirculation and no difference in methane production
220 was found between treatments. However, the pH, alkalinity, total acids concentration
221 (Fig. 2c&d) and ammonia concentration (Fig. 3b) increased from 7.34 ± 0.02 for A to
222 7.52 ± 0.02 for Ar, from 3.50 ± 0.54 g/L to 5.94 ± 0.76 g/L, from 0.98 ± 0.30 g/L to $1.55\pm$
223 0.56 g/L and from 378 ± 70 mg/L to 760 ± 177 mg/L, with an increasing rate of 2 %, 70 %,
224 58 % and 101 %, showing the throttling effect of liquid digestate recirculation on
225 alkalinity, acids and ammonia, the same with A and Ar. Among the above parameters,
226 only the alkalinity of B showed a significant decrease trend ($P<0.05$). According to the
227 formula of its trend line [$y=-0.025x+4.376$, $R^2=0.7256$, where y is alkalinity (g/L), and x
228 is time (d)], the alkalinity of digester B will decline to 2.0 g/L by the 95th day of
229 digestion, at which time, the stability of digester B would collapse just as in digesters A
230 and Ar. Whereas, risk of fermentation failure cannot be predicted in digester Br based on
231 available data at present, showing a good effect of recirculation on the stability of

232 digesters fed with CS:PM 3:1.

233 In summary, the improved effect of liquid digestate recirculation occurs in the
234 fermentation system characterized by a lack of VFA, buffering capacity, and specific
235 nutrients. Usually, this kind of fermentation system is caused by feedstock that is
236 relatively difficult to degrade and imbalance in nutrients, such as crop straw. And the
237 reason for the improvement is to alleviate the loss of insufficient substances through
238 recirculating liquid digestate to make full use of the limited substances and render high
239 performance.

240 3.1.2 Inhibited effects of recirculation under 1:1, 1:3, and PM

241 The dynamics of daily methane production and proportion of the digesters fed by
242 CS:PM 1:1 (C and Cr), 1:3 (D and Dr), and only PM (E and Er) without and with liquid
243 digestate recirculation are shown in Fig. 1c-e. Among these six treatments, only digester
244 C (1:1 without recirculation) performed stable and efficient after start-up till the end. No
245 significant change trend ($P>0.05$) was found in methane production, VFAs, alkalinity,
246 and ammonia concentration, indicating the equilibrium between hydrolysis, acidification,
247 and methanogenesis in digester C. However, the balanced state of fermentation was
248 disturbed by liquid digestate recirculation shown as VFAs, alkalinity, and TAN
249 cumulated in Cr over time. Imbalanced digestion also occurred in Cr, D, Dr, E, and Er.
250 The methane production of these digesters went through four periods: start-up period,
251 stable period 1, decline period, and stable period 2. For digesters Cr, D, Dr, E and Er, the
252 methane production in stable period 2 was 24 %, 19 %, 85 %, 73 %, and 93 % lower

253 than that in stable period 1, indicating these digesters were in an inhibited state. The
254 methane production in stable period 2 in digesters with liquid digestate recirculation was
255 only 77 %, 18 % and 23 % of the methane production in stable period 2 in digesters
256 without recirculation under CD: PM 1:1, 1:3 and only PM, which reflected the
257 aggravated inhibition with liquid digestate recirculation.

258 Unlike methane production, the dynamics of VFAs, alkalinity, pH (Fig. 2f-j), and
259 ammonia concentration (Fig. 3c-e) in digesters Cr, D, Dr, E, and Er couldn't be divided
260 into periods, but continuously changed over time. The reason to this asynchrony is that
261 inhibitors need to accumulate to exceed limits before they exert their inhibitory effect. In
262 anaerobic digestion, ammonia is an essential nutrient for microbial growth and a good
263 buffer for digester stabilization when it is in an appropriate dose. But when ammonia
264 accumulated to a relatively high dose, it becomes an inhibitor to restrict methanogenesis
265 ((Rajagopal et al., 2013; Wang et al., 2016). In this study, whether with liquid digestate
266 recirculation or not, when the TAN above 1,500 mg/L, and FAN above 50 mg/L, the
267 corresponding methane production ended the stable period 1 and entered to the decline
268 period. The duration of stable period 1 in digesters with liquid digestate recirculation
269 was shorter than that without recirculation under the same feedstock condition,
270 indicating inhibitors were enriched by liquid digestate recirculation.

271 It is accepted that ammonia strongly inhibited methanogenesis but minimally
272 affected hydrolysis and acidification, as a result to which, VFAs accumulation will occur
273 (Rajagopal et al., 2013; Wang et al., 2016). The concentration of acetic acid, propionic

274 acid, and butyric acid increased along with the increase of TAN. The increased VFAs
275 usually results in a decrease in pH and further limits methanogenesis activity, just like
276 the final rancidity of A and Ar. However, in Cr, D, Dr, and E, VFAs, alkalinity and
277 ammonia neutralized each other so that the pH did not decrease. The interactions
278 between VFA, alkalinity, and ammonia led to an inhibited steady-state (Li et al., 2015),
279 where the pH was in the suitable range recommended by literature for the anaerobic
280 digestion (Chen et al., 2008), but methane production remained relatively stable in an
281 inefficiency state, shown as the stable period 2 in these inhibited digesters. These results
282 were in agreement with those of former investigations conducted by Huang et al. (2015)
283 and Wu et al. (2016). It is noteworthy that butyric acid, which is an important chemical
284 raw material and organic intermediate (Fu et al., 2017), counted over 55 % of the
285 cumulated VFAs in digesters Cr, D, Dr, E, and Er. The role of accelerated VFA
286 accumulation through liquid digestate recirculation might be performed with further
287 research to benefit the biological production of butyric acid.

288 In summary, the recirculation of liquid digestate in digesters, which is in
289 equilibrium and steady-state, will break the balance and cause accumulation and then
290 come to the inhibition. Identically, the recirculation of liquid digestate in digesters,
291 which is in excessive and accumulation state, will accelerate accumulation and lead to
292 aggravated inhibition. As in this study and previous studies, the main inhibitor turned
293 out to be the accumulation of ammonia when performing recirculation in digesting
294 animal manure. Other inhibitors, such as TS accumulation (Estevez et al., 2014) and

295 increased viscosity (Ni et al., 2017), were also found to be the main cause of inhibition
296 in a few types of research.

297 3.1.3 Interaction of feeding ratios and liquid digestate recirculation

298 Cross comparison by cluster analysis and principal component analysis (PCA) was
299 conducted on gas production and proportion as well as the internal digestion parameters
300 of all the digesters.

301 Cluster analysis divided the digestion strategies into four categories (Fig. 4a).
302 Digesters A, Ar, and B were clustered together because their nitrogen (TAN<500 mg/L)
303 and buffer (alkalinity<10 g/L) content were low and declining over time. Digesters C
304 and Br were clustered because of the excellent performance in both gas production and
305 system stability. Digesters D and Cr were clustered as the slightly inhibited group, and
306 the digesters E, Dr, and Er were clustered as the seriously inhibited group.

307 From the perspective of the influent of digesters, the changes in feeding ratios and
308 the use of digestate recirculation are both measures of changing influent composition.
309 The high carbon to nitrogen ratio (C/N ratio) of crop straw could lead to an imbalance in
310 nutrients and a lack of buffering capacity (Neshat et al., 2017; Sawatdeenarunat et al.,
311 2015). And the low C/N ratio of animal manure could cause the inhibition of ammonia
312 accumulation (Rajagopal et al., 2013). So the different straw-to-manure ratios formed a
313 C/N gradient from high to low in influent from digester A to E. If the recirculated liquid
314 digestate was regarded as a co-substrate just like CS and PM, the C/N ratio of influent
315 was changed by exchanging CS-PM-water influent to CS-PM-digestate influent through

316 liquid digestate recirculation. When calculated the C/N ratios of influent from the
317 composition of raw materials and liquid digestate, the C/N ratios of influent in
318 recirculated digesters were 1.3-3.2 lower than that in digesters without recirculation
319 (Table S1), because some carbon in raw materials has dissipated as CH₄ and CO₂ while
320 little nitrogen has gone as NH₃. All recirculation digesters were clustered with
321 non-recirculation digesters which were fed with more CS and less PM, namely Br with
322 A, Cr with B, Dr with C and Er with D, because their similar C/N ratios could service
323 similar nutrition and environment for anaerobic organisms. When the C/N ratio of the
324 raw material is higher than the suitable range, the C/N ratio of the new substrate
325 composed of liquid digestate will be closer to the suitable range, or enter the suitable
326 range, providing more balanced nutrients for microorganisms and obtaining more
327 efficient digestion process. Similarly, when the C/N ratio of raw material is lower than
328 the appropriate range, the recirculated liquid digestate will make the C/N ratio of the
329 new substrate lower and farther away from the appropriate range, resulting in a greater
330 imbalance in digesters. Based on this, liquid digestate recirculation is more suitable in
331 anaerobic digestion of materials with a slightly high C/N ratio (a C/N of 25 in this study),
332 such as lignocellulosic materials.

333 The results of PCA closely complemented those of cluster analysis (Fig. 4b). The
334 four performance groups shown by cluster analysis (inadequate, well-run, mildly
335 inhibited and severely inhibited), could be clearly positioned across the arched
336 distribution. The proportion of CS gradually decreases and PM increases along the arch

337 from left to right. The points that are positioned at the left-hand end of the arch reflected
338 a shortage of buffering matter, while the points lying at the right-hand end of the arch
339 reflected inhibition by ammonia and accumulation of organic acids, indicating that the
340 lignocellulosic materials tends to the digestion performance type of inadequate, while
341 livestock manure tends to the type of excessive. The factor loading plot for the PCA is
342 presented in Fig. 4c. Alkalinity, TAN and FAN contribute to the positive direction of
343 principle component 1 (PC1) and principle component 2 (PC2). All acids contribute to
344 the positive direction of PC1 and negative direction of PC2. If a point moves close to the
345 positive direction of PC1 it means both acid and alkali increase, and if a point moves
346 close to the negative direction of PC1 it means a decrease in acid and alkali. Liquid
347 digestate recirculation moved the distribution of all feedstock mixtures to the right,
348 among which only CS (A and Ar) was moved right and upwards while 1:1 (C and Cr),
349 1:3 (D and Dr) and only PM (E and Er) were moved right and downwards (Fig. 4d). The
350 results indicated that the effect of liquid digestate recirculation on anaerobic digestion
351 under all tested feedstock conditions is to increase alkalinity, ammonia and organic acids
352 concentrations. For digesters in inadequate state such as digesters fed with CS or CS:PM
353 3:1, the increasing of alkali and acid by recirculation relieved or eliminated the shortage.
354 While for digesters in balance or excessive state such as digesters fed with CS:PM 1:1,
355 1:3 and PM alone, the increasing of alkali and acid by recirculation triggered or
356 aggravated the accumulation of ammonia and VFA, causing subsequent adverse
357 fermentation performance.

358 In summary, feeding ratios and digestate recirculation both are measures to change
359 influent. Different feeding ratios from CS to PM provided different C/N ratio from high
360 to low for the digesters, and formed different levels of metabolites from inadequate to
361 accumulated. On the basis of feeding ratios, liquid digestate recirculation played a role
362 in reducing the C/N ratios of influent, and recycling parts of metabolites, and benefited
363 digesters with high C/N and inadequate metabolites, inhibited digesters with low C/N
364 and accumulated metabolites.

365 3.2 Effects of feeding ratios and recirculation on microbial community

366 Anaerobic digestion is conducted by a community of microbes. To further
367 understand the microbial responses to feeding ratios and liquid digestate recirculation,
368 microbial analysis by Illumina MiSeq sequencing were carried out. The relationship
369 between fermentation parameters and microbial community was analyzed by
370 redundancy analysis (RDA). The detailed microbial community structure of
371 methanogens and the correlations between factors and methanogens was shown and
372 discussed.

373 3.2.1 Summary of the observed sequence

374 The summary of microbial analysis including richness and diversity indexes were
375 in Table S2. Corresponding to the fermentation performance of digesters, inhibited
376 digesters (Cr, D, Dr and E) showed lower richness and diversity in bacterial community,
377 which was indicated by less OTUs and species, lower Chao and Shannon indices, and
378 higher Simpson indices in digesters Cr, D, Dr and E than in digesters Ar, B, Br and C. In

379 terms of archaea, this difference between uninhibited and inhibited digesters was not
380 obvious, but the diversity of archaea in digester C, which produces the highest methane
381 yield, was lower than that of other digesters, indicating the methane metabolism of high
382 efficient digesters was relatively pure and simple.

383 3.2.2 Redundancy analysis

384 The relationship between fermentation parameters and microbial community was
385 analyzed by redundancy analysis (RDA) (Fig. 5). When the digester points were
386 projected perpendicularly onto the arrow of CS and PM, the projections of digesters
387 with liquid digestate recirculation located closer to the positive end of PM and further to
388 the negative end of CS than digesters fed by the same feedstock ratios but without liquid
389 digestate. The microbial community structure changed to that of more PM and less CS
390 under the influence of liquid digestate recirculation, which was corresponding to the fact
391 summarized from the fermentation performance data. Among all the fermentation
392 parameters, the arrows of TAN and propionic acid were the longest in Fig 5a, indicating
393 the major effects of TAN and propionic acid to bacterial community changes. While, the
394 arrows of TAN and Alkalinity were the longest in Fig 5b, indicating their major impacts
395 on archaeal community dynamics. The different straw/manure ratios in feedstock caused
396 the varying amount of flow-in nitrogen and then resulted in difference in TAN. The
397 discharge or recirculation of liquid digestate caused the change in the amount of
398 flow-out TAN. Then, under the major effect of different TAN, the microbial community
399 evolved into different structure and formed different digester performance types.

400 Bacteria species from phylum of Firmicutes, Cloacomonetes, Tenericutes and
401 Proteobacteria; Methanogens from genus of Methanoculleus, Methanosarcina,
402 Methanobrevibacter, Methanosphaera and Methanobacterium survived the high TAN
403 environment, and formed the methanogenic metabolism under severely inhibition of
404 ammonia.

405 3.2.3 Microbial community structure

406 The community structures of archaea at genus level were shown in Fig. 6a.
407 Combined with digester performance, the dominant methanogen in digester Ar were
408 Methanocorpusculum (19.3 %) and Methanosaeta (18.7 %), and the unique archaeal
409 community of digester Ar corresponded to its inadequate and out-run state. The
410 dominant methanogen was Methanosaeta in digesters B (51.8 %), Br (51.9 %), C
411 (83.4 %) and Cr (67.3 %), and these digesters were all in steady methane production.
412 However, digesters B, Br and C was in steady-state from beginning, but digester Cr was
413 in steady-state after mildly inhibition. Corresponding to the slightly inhibition in
414 digester Cr, Methanobacterium (12.4 %), Methanosphaera (7.2 %) and Methanosarcina
415 (5.9 %) in digester Cr were enriched. In digesters D, Dr and E, which were also in the
416 fermentation state of inhibitory, Methanosarcina was abundant, accounted 41.2 % for D,
417 32.1 % for Dr and 49.7 % for E. In addition, Methanosphaera, Methanobrevibacter,
418 Methanoculleus were more abundant in digesters D, Dr and E than in other digesters. An
419 interesting phenomenon was that the relative abundance of Methanosaeta were 35.4 %
420 and dominant in archaea in the severely inhibited digester Dr with the TAN of 3,000

421 mg/L. However, it has been widely reported that Methanosaeta are sensitive to high
422 ammonia concentrations (Wilson et al., 2012; Zamanzadeh et al., 2016). In the study by
423 Zamanzadeh et al. (2016) on anaerobic digestion of food waste, the digester with liquid
424 digestate recirculation also had a higher relative abundance (91 %) of Methanosaeta than
425 that of digesters without recirculation (65 %) under mesophilic condition. It was
426 speculated that the toxicity of ammonia to Methanosaeta was relieved in digesters with
427 liquid digestate recirculation.

428 The relationship between fermentation parameters and methanogens was shown in
429 Fig. 6b by correlation analysis. Among all the parameters, the percentage of CS in
430 feedstock showed the significant correlation ($P < 0.05$) with methanogens from 6 genera,
431 indicating the change in feeding ratios was one of the main factors that led to change in
432 methanogen community structure. Also, TAN was one of the main factors who showed
433 significant correlation ($P < 0.05$) with methanogens from 5 genera. Methanogens from
434 genus of Methanoculleus, Methanosarcina, Methanobrevibacter, and Methanosphaera
435 showed significant positive correlation ($P < 0.05$) with concentrations of acids and
436 ammonia, which was consistent with results from RDA, and showing the tolerance of
437 these methanogens under inhibition of acids and ammonia accumulation.

438 The changes in bacteria community structure were not as dramatic as methanogens.
439 (Fig. S1). Firmicutes and Bacteroidetes accounted for over 60 % of the total bacteria and
440 were dominant phylums in all digesters, and the relative abundance of Firmicutes
441 gradually increased along with the proportion of CS decreased in feedstock. TAN was

442 the main factor in changing bacteria community structure because TAN showed
443 significant correlation with 12 bacterial phyla among the top 14 phyla.

444 In summary, the microbial community structure varied corresponding to the
445 fermentation state. The dominant methanogens in the well-run digesters were
446 Methanosaeta, while Methanosarcina and Methanosphaera dominated in the inhibited
447 digesters. TAN was the main factor in microbial dynamics. And liquid digestate
448 recirculation might relieve the toxicity of ammonia to Methanosaeta in inhibited
449 digester.

450 3.3 Benefits analysis

451 In order to quantify the benefits of liquid digestate recirculation, the consumption
452 and emission data under the same energy output were calculated based on the data in
453 this study from the best process without recirculation (digester C, marked as convention
454 mode) and the best process with recirculation (digester Br, marked as recirculation mode)
455 (Table 3). The discharge of liquid digestate of recirculation mode was reduced by 81.9 %
456 compared to that of convention mode, and soluble chemical oxygen demand (sCOD)
457 emission was reduced by 70.4 %. The water consumption (water used in diluting
458 feedstock into desired influent TS) of recirculation mode was cut down by 65.4 % of
459 convention mode. The warm liquid digestate, instead of water at ambient temperature
460 mixed with raw materials, could reduce the heat needed to raise the influent to the
461 fermentation temperature due to heat recovery. According to the equation expressed by
462 Wang et al. (2018), the theoretical heat required to raise the influent to fermentation

463 temperature in recirculation mode was 56.3 % lower than that in convention mode,
464 reducing the influent heat load from 9.7 % to 4.2 % of total energy production (energy
465 of total produced biomethane). The reduced water consumption and influent heat load in
466 recirculation mode, on the one hand, marked the contribution of recirculation in saving
467 resource and energy; on the other hand, indicated the benefits of cost-saving. Under the
468 buying water price of 2-7 CNY and the selling biomethane price of 2-4 CNY, the saved
469 cost in the recirculation mode of water and heat was 7.1-15.7 % of total revenue from
470 sales of biomethane.

471 When scaled up to daily biomethane production of 10,000 m³ and compared to
472 convention mode, the recirculation mode could reduce the discharge amount of liquid
473 digestate of 335.7 t/d, reduce sCOD emission of 1.22 t/d, save water of 280 t/d and
474 theoretically recover heat from liquid digestate of 19.0 GJ/d, showing the advantages of
475 recirculation mode in reducing pollutant, saving resource and energy, and reducing cost.
476 However, a more detailed calculation is needed under a certain situation and include the
477 cost of handling raw material and solid digestate which have huge regional differences.

478 As a potential benefit, the production time and amount of liquid digestate might be
479 controlled by changing proportions of agricultural waste in feedstock and selectively
480 employing liquid digestate recirculation while ensured efficient production of renewable
481 methane. A new operation strategy of alternate using CS:PM 3:1 with recirculation (Br)
482 and CS:PM 1:1 without recirculation (C) could be performed in the same one digester,
483 and run C when liquid digestate was needed while run Br when not needed. The

484 integrated approach will achieve on-demand production of liquid digestate and facilitate
485 downstream utilization of liquid digestate for seed germination promotion (Aihemaiti et
486 al., 2019), pest control and growth regulation (Li et al., 2016) in the seasonal
487 agricultural process, which will achieve high value utilization of liquid digestate and
488 promote sustainable development of agriculture.

489 3.4 Production recommendation

490 Liquid digestate recirculation provides a possibility of not discharging continuously
491 produced, large amounts of liquid digestate in scaled biomethane projects, which attracts
492 the attention of practitioners and researchers. However, because of the difference of raw
493 materials and processes, the liquid digestate obtained is also very different, which makes
494 the recirculation of liquid digestate perform different effects under different situation.
495 The possible negative effects of recirculation restrict its popularization and application.
496 The interaction between feedstock formula and liquid digestate recirculation on
497 anaerobic digestion was investigated in this study. Results indicated that recirculation
498 was a process to reduce material loss from digesters. For this reason, the improved effect
499 of recirculation occurred in digesters that were lack of nutrients and buffers, while the
500 inhibited effect occurred in digesters that were abundance of nutrients and buffers. Since
501 the inhibitory effect of liquid digestate recirculation is caused by inhibitor accumulation,
502 the inhibition is not immediately apparent with the beginning of recirculation. In the
503 process of liquid digestate recirculation, it is recommended to grasp the changing trend
504 of possible inhibitors to keep high efficient and to adjust in time.

505 As under the same operation condition of this study, digesters fed by more-straw
506 feedstock performed into inadequate state and improved by liquid digestate recirculation
507 while digesters fed by more-manure feedstock performed into excessive state and
508 inhibited by liquid digestate recirculation. In addition, both the fermentation parameters
509 and the microbial analysis indicated that digesters with liquid digestate recirculation
510 were similar to those without liquid digestate recirculation but fed by more manure and
511 less straw. That is, if the liquid digestate recirculation will be applied to a well-run
512 digester, it is necessary to adjust the feedstock formula, appropriately increase the
513 proportion of straw and reduce the proportion of manure, to match the liquid digestate
514 recirculation so as to avoid inhibitor accumulation and achieve desired performance.
515 And the appropriate proportion under conditions of this study was 25 %. Conversely,
516 some external conditions may cause the raw materials to change, such as the manure in
517 the area is not enough to be used as co-digestion material, or the straw is eager to be
518 disposed of because of the seasonal harvest. If a well-run digester had to change
519 feedstock formula to fed by less manure or more straw, the liquid digestate recirculation
520 is recommended to be introduced to make full use of buffers and nutrients to match the
521 change in feedstock formula.

522 This study focused on the response of digestion performance to liquid digestate
523 recirculation under different feedstock conditions with uniform process conditions,
524 rather than optimize the recirculation process of different feedstock conditions. So, the
525 final failure or decline of methane production occurred in digesters fed by only CS,

526 CS:PM 1:3, and only PM. However, it is worthwhile to further study the optimization of
527 liquid digestate recirculation under these feedstock conditions and other types of raw
528 material in the future, which is conducive to reducing the discharge of liquid digestate
529 from the source and making full use of water, heat, and substances in liquid digestate.
530 Li et al. (2018) and Peng et al. (2016) also studied the effect of liquid digestate
531 recirculation on digesting CS, pretreatment methods (NaOH), buffering agents
532 (NaHCO_3), and longer HRT (40-45 d) were used, which could make straw easier to
533 degrade, provide better conditions, and more time for microorganisms to degrade. As a
534 result, no process failure occurred, and long-term, stable, and efficient fermentation was
535 achieved. An integrated approach including pretreatment, pH control, liquid digestate
536 recirculation, etc. may be a potential scheme to solve the problem of mono-digestion of
537 crop straw in areas where manure and other co-digestion materials are scarce.

538 In studies on liquid digestate recirculation in manure digesters, appropriate
539 interventions were introduced to reduce the negative impact of liquid digestate
540 recirculation on digesting animal manure and provide the possibility of ensuring both
541 high efficient digestion and the long-term operation of recirculation. In a study by Nie et
542 al. (2015) on mono-digesting chicken manure with liquid digestate recirculation, 72 %
543 of ammonia in liquid digestate was removed through decompression steam stripping
544 before recirculation, and long-term stable digestion was achieved. Besides, air stripping
545 was used by Wu et al. (2016) to mitigate ammonia in liquid digestate before
546 recirculation in anaerobic digestion of chicken manure. Results showed the ammonia

547 concentration in digester was declined after ammonia stripping of liquid digestate, and
548 methane yield was back to the same level as the control digester without recirculation.
549 However, either vacuum stripping or air stripping requires additional equipment and
550 operation costs, which limits these technologies to be promoted. Further research is
551 needed to reduce costs and simplify operation.

552 Some studies have been optimized and explored the more detailed process
553 optimization, including recirculation ratio (partially recirculation) (Ratanatamskul and
554 Saleart, 2016; Zuo et al., 2015), pre-mixing time of liquid digestate with raw material
555 before recirculation (Elsayed et al., 2019; Liu et al., 2019), etc., to achieve high efficient
556 digestion with liquid digestate recirculation. In this way, the liquid digestate
557 recirculation will have the potential to be applied under a wider variety of raw material
558 conditions and operating processes. And the advantage of controllable discharge of
559 liquid digestate, waste reduction, and water conservation of liquid digestate recirculation
560 will benefit more regions and people.

561 **4 Conclusions**

562 Ten lab-scaled semi-continuous anaerobic digesters, fed by corn stalk, pig manure,
563 and their 3:1, 1:1, 1:3 mixtures, with or without liquid digestate recirculation, performed
564 as four states of inadequate, well-run, mildly inhibited and severely inhibited. Methane
565 production was promoted by recirculation when fed with corn stalk and 3:1, while
566 inhibited under 1:1, 1:3 and pig manure. Microbial community varied to their
567 performance states. The regimes of 3:1 with recirculation and 1:1 without recirculation

568 outperformed the other digesters, and their dominant methanogens were Methanoseata.
569 Recirculation mode showed 81.9 % liquid digestate reduction, 70.4 % COD reduction,
570 and 65.4 % water saving to that of convention mode, which achieving efficient and
571 cleaner biomethane production.

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- 725
726

727 Table 1.

728 Characteristics of corn stalk (CS), pig manure (PM) and inoculum.

729

Parameter	Unit	Corn stalk	Pig manure	Inoculum
Moisture content	% Wet weight	8.58±0.33	68.20±0.57	93.14±0.42
Total solids	% Wet weight	91.42±0.31	31.80±0.41	6.86±0.34
Volatile solids	% Total Solids	98.55±0.18	78.00±0.23	58.93±0.19
Hemicellulose	% Total Solids	30.47±0.01	14.56±0.04	11.56±0.02
Cellulose	% Total Solids	34.08±0.19	9.28±0.44	13.76±0.03
Total carbon	% Total Solids	61.81±0.62	47.02±1.08	40.39±0.07
Total nitrogen	% Total Solids	1.22±0.00	4.78±0.00	1.86±0.00
C/N ratio		50.7±0.7	9.8±1.13	21.8±0.00
pH		Not determined	7.7±0.0	7.5±0.0
Average±standard deviation (n=3)				

730

731

732

733 Table 2.

734 Experimental design in this study.

735

Setup	Feedstock (or CS:PM ^a)	C/N Ratio ^b	Liquid digestate	Name ^c in the study
1	Only CS	50.7	Discharge	A
2	Only CS	50.7	Recirculation	Ar
3	3:1	25.2	Discharge	B
4	3:1	25.2	Recirculation	Br
5	1:1	16.7	Discharge	C
6	1:1	16.7	Recirculation	Cr
7	1:3	12.4	Discharge	D
8	1:3	12.4	Recirculation	Dr
9	Only PM	9.8	Discharge	E
10	Only PM	9.8	Recirculation	Er

a. The CS:PM is the ratio of corn stalk to pig manure in feedstock, and is based on volatile solid (VS) content.

b. Calculated from proportion and composition of raw material

c. The letter “r” represents recirculation.

736

737

738

739 Table 3.

740 Comparison of emission and consumption per unit energy output between convention

741 mode (based on digester C) and recirculation mode (based on digester Br).

	Unit	Convention mode	Recirculation mode	Difference ^a
Energy output	GJ	1	1	0.0 %
Biomethane ^b	m ³	27.9	27.9	0.0 %
Revenue of selling gas ^c	CNY	57.5-115.0	57.5-115.0	0.0 %
Influent				
Corn stalk	kg ^d	68.8	112.4	-63.3 %
Pig manure	kg	249.9	136.8	45.3 %
Clean water	m ³	1.23	0.43	65.4 %
Liquid digestate	m ³	0.00	1.01	--
Effluent				
Solid digestate ^e	kg	387.5	470.9	-21.5 %
Liquid digestate	m ³	1.16	1.22	-5.2 %
-Recirculation	m ³	0.00	1.01	--
-Discharge	m ³	1.16	0.21	81.9 %
-sCOD discharge	kg	5.00	1.48	70.4 %
Heat required ^f	GJ	0.097	0.042	56.3 %
Methane required	m ³	2.70	1.18	56.3 %
Clean water cost ^g	CNY	2.5-8.6	0.9-3.0	65.4 %
Heat cost ^h	CNY	5.4-10.8	2.4-4.7	56.3 %
Sum of water and heat cost	CNY	8.0-19.7	3.3-7.8	58.0-61.9 %
Proportion of cost in revenue	%	12.2-25.4	5.1-9.7	58.0-61.9 %

a. Difference was calculated as $(x-y)/x*100\%$, where x is the value of convention mode and y is value of recirculation mode.

b. 1 GJ energy is converted from 27.9 m³ biomethane, the heat value of which is 35.9 MJ/m³.

c. Gas sold is bio-natural gas with a methane proportion of 97 %, and the price is 2-4 CNY according to practice in China.

d. The values, which are united by kg, are based on wet weight.

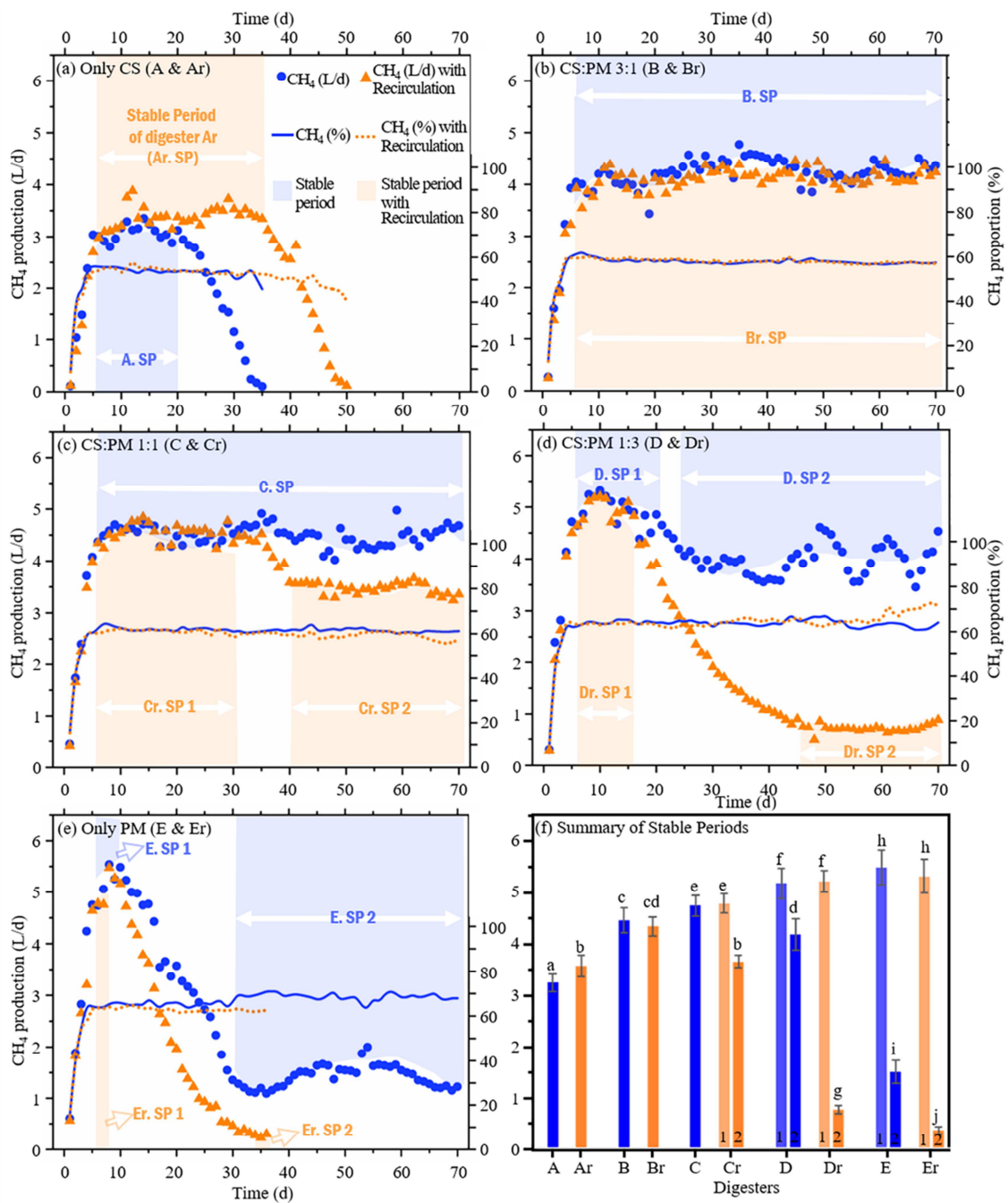
e. The moisture content of solid digestate is 78.8 % after solid-liquid separation.

f. Heat required to raise the influent to fermentation temperature (35 °C). The ambient temperature is assumed as 20 °C.

g. The commercial water price is assumed 2-7 CNY according to practice in China.

h. Heat cost is calculated as the reduced income of selling biomethane by the combustion of biomethane to obtain these heat.

742



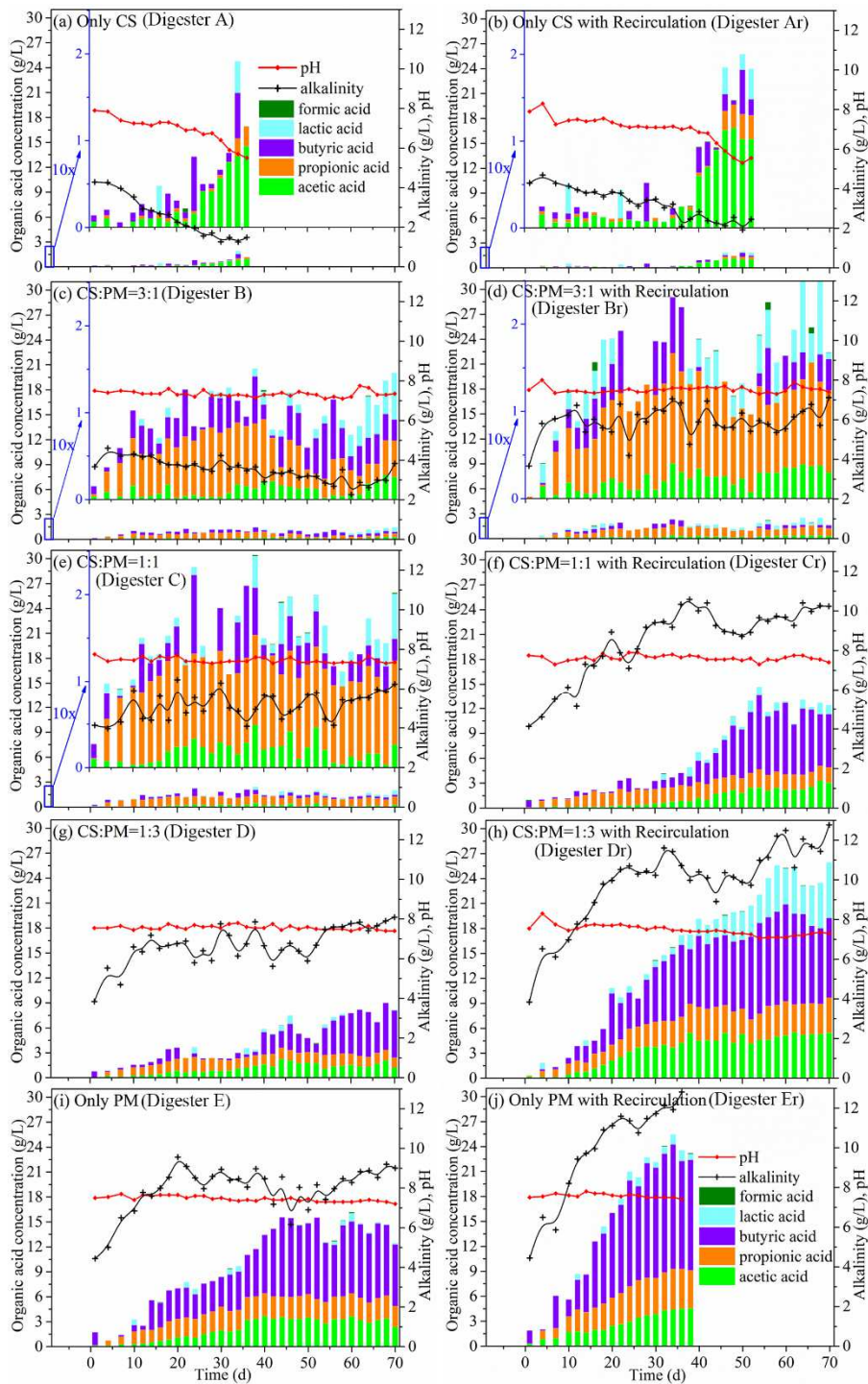
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744 Fig. 1. Methane production (scatters) and proportion (lines) without (blue) or with

745 (orange) liquid digestate recirculation (a-e). And bar chart (f) shows the average

746 methane production of stable periods (periods that covered by shadows in a-e).

747



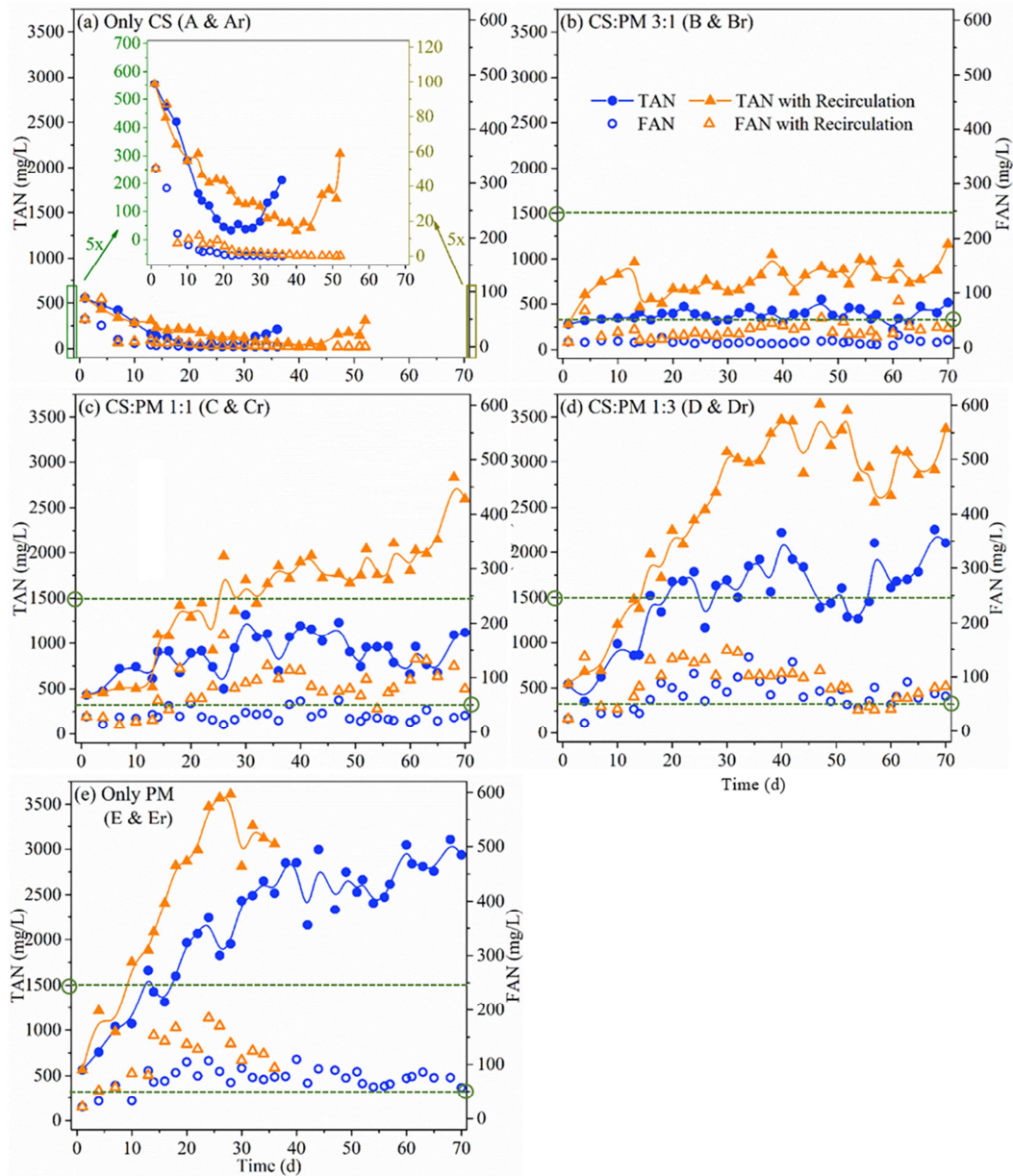
748

749 Fig. 2. Changes of pH (red symbol-line, dot), alkalinity (black symbol-line, cross) and

750 organic acids (acetic, propionic, butyric, lactic, formic which are represented as five

751 colored and stacked columns) concentrations.

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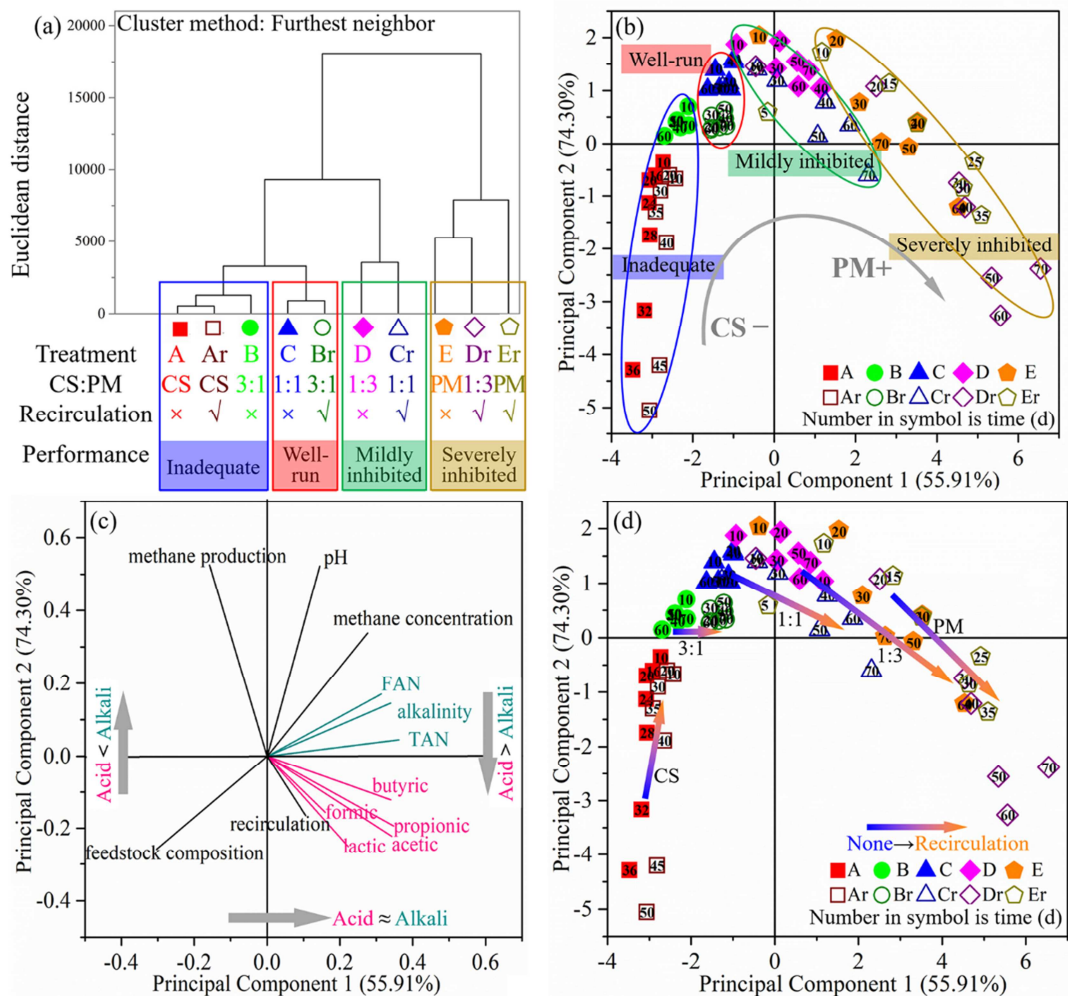


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754 Fig. 3. Total ammonia (TAN), free ammonia (FAN) concentrations (symbol-lines)

755 without (blue circle) or with (orange triangle) liquid digestate recirculation.

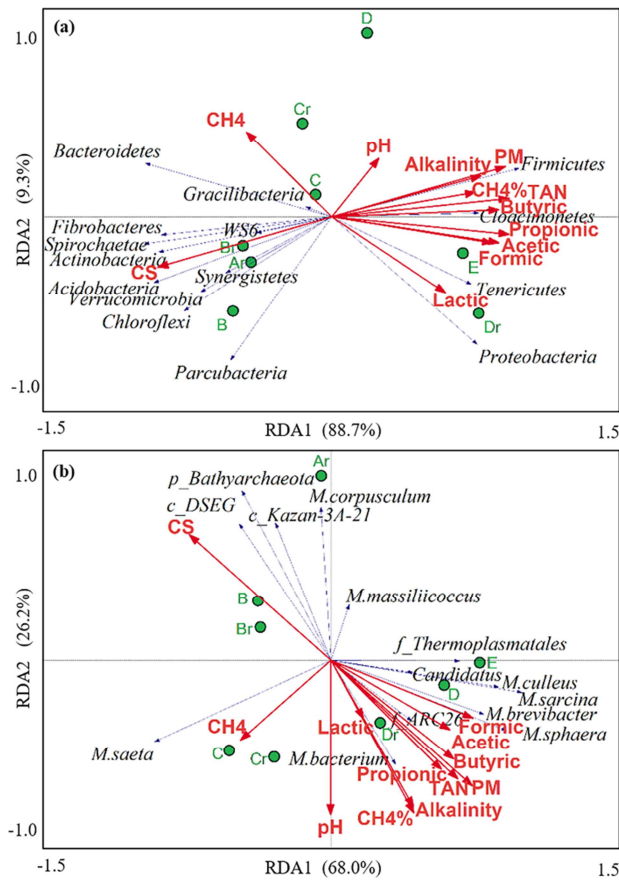
756



757

758 Fig. 4. Cross comparison by [a] cluster analysis where ten digesters are clustered into
 759 four performance types of inadequate, well-run, mildly inhibited and severely inhibited;
 760 and by [b] principal component analysis (PCA). [c] The factor loading plot for PCA. [d]
 761 Position changes in PCA caused by liquid digestate recirculation.

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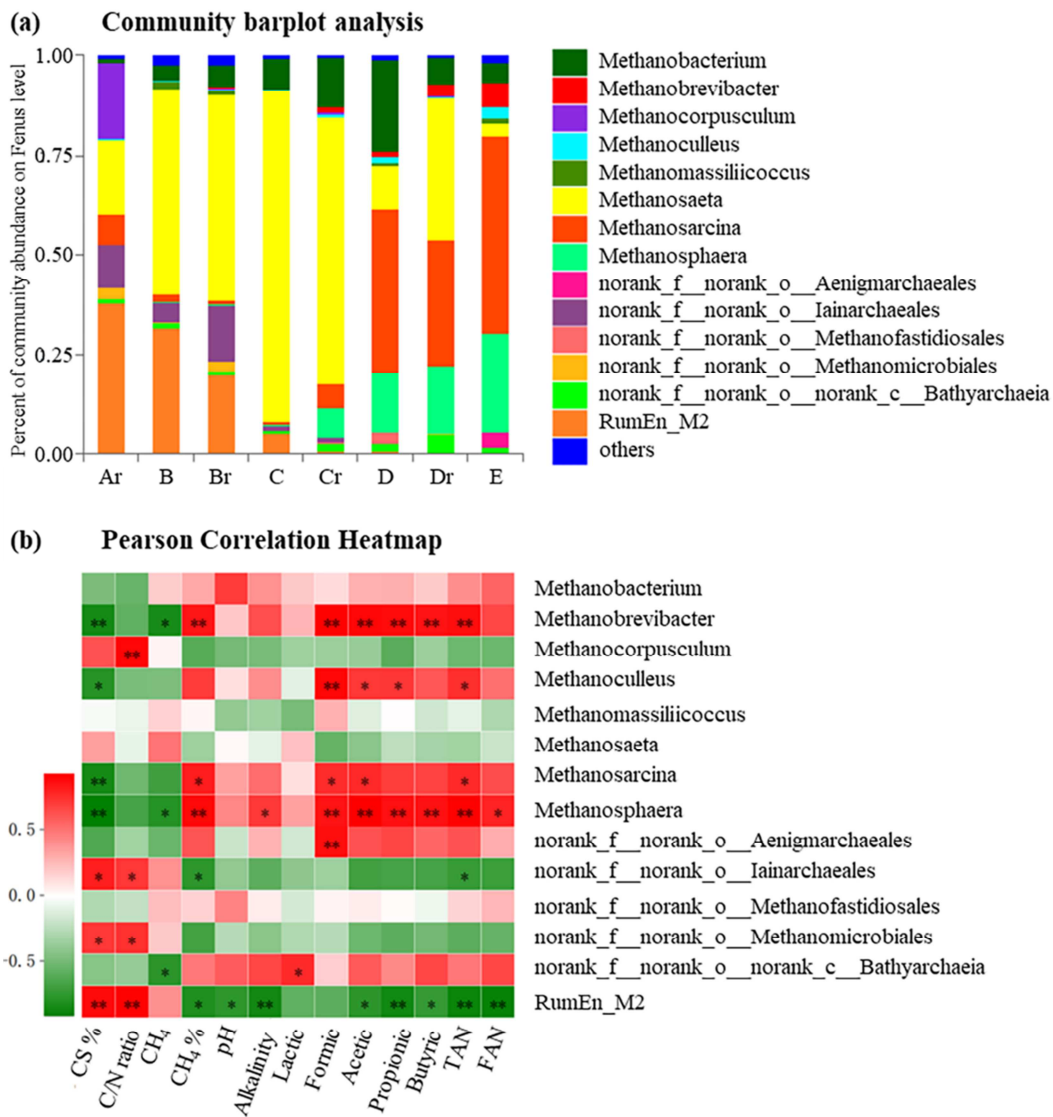


763

764 Fig. 5. Redundancy analysis of bacteria on phylum level (a) and archaea on genus level

765 (b) with fermentation parameters.

766



Highlights

- Cross effects of liquid digestate reuse and feed-formula on performance and microbes.
- Recirculation is beneficial when straw to manure ratio is 3:1 or higher in feedstock.
- Recirculation mode ran well and reduced 81.9% liquid discharge and 65.4% water usage.
- Cooperation of feedstock and recirculation may achieve controllably liquid discharge.

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Declaration of interests

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

The authors declare the following financial interests/personal relationships which may be considered as potential competing interests:

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