TOPICAL REVIEW • OPEN ACCESS

Meso scale component manufacturing: a comparative analysis of non-lithography and lithography-based processes

To cite this article: Azfar Khalid et al 2022 J. Micromech. Microeng. 32 063002

View the article online for updates and enhancements.

You may also like

- <u>Motility-induced clustering and meso-scale</u> <u>turbulence in active polar fluids</u> Vasco M Worlitzer, Gil Ariel, Avraham Be'er et al.
- <u>SA-based concrete seismic stress</u> monitoring: a case study for normal strength concrete S Hou, H B Zhang and J P Ou
- <u>Information content: Assessing mesoscale structures in complex networks</u> M. Zanin, P. A. Sousa and E. Menasalvas



IOP ebooks[™]

Bringing together innovative digital publishing with leading authors from the global scientific community.

Start exploring the collection-download the first chapter of every title for free.

IOP Publishing

J. Micromech. Microeng. 32 (2022) 063002 (21pp)

Topical Review

Meso scale component manufacturing: a comparative analysis of non-lithography and lithography-based processes

Azfar Khalid^{1,*}, Yang Wei¹, Muhammad Rizwan Saleem^{2,3} and Waqas Akbar Lughmani⁴

¹ Department of Engineering, School of Science & Technology, Nottingham Trent University, NG11 8NS Nottingham, United Kingdom

² University of Eastern Finland, Institute of Photonics, PO Box 80101, Joensuu, Finland

³ School of Chemical & Materials Engineering, National University of Science & Technology, Islamabad, Pakistan

⁴ Department of Mechanical Engineering, Capital University of Science & Technology (CUST), Islamabad, Pakistan

E-mail: azfar.khalid@ntu.ac.uk

Received 23 August 2021, revised 19 February 2022 Accepted for publication 28 April 2022 Published 12 May 2022



Abstract

The paper identifies the meso scale (10 μ m to few millimeters) component size that can be manufactured by using both lithography and non-lithography based approaches. Non-lithography based meso/micro manufacturing is gaining popularity to make micro 3D artifacts with various engineering materials. Being in the nascent stage, this technology looks promising for future micro manufacturing trends. Currently, lithography based micro manufacturing techniques are mature, and used for mass production of 2D, 2.5D features and products extending to 3D micro parts in some cases. In this paper, both the techniques at state-of-the-art level for meso/micro scale are explained first. The comparison is arranged based on examples and a criterion is set in terms of achievable accuracy, production rate, cost, size and form of artifacts and materials used. The analysis revealed a third combined approach where a mix of both techniques can work together for meso scale products. Critical issues affecting both the manufacturing approaches, to advance in terms of accuracy, process physics, materials, machines and product design are discussed. Process effectiveness guideline with respect to the component scale, materials, achievable tolerances, production rates and application is emerged, as a result of this exercise.

* Author to whom any correspondence should be addressed.

Original content from this work may be used under the terms of the Creative Commons Attribution 4.0 licence. Any further distribution of this work must maintain attribution to the author(s) and the title of the work, journal citation and DOI. Keywords: non-lithography, lithography, micro/meso scale manufacturing

(Some figures may appear in colour only in the online journal)

1. Introduction

The integration density of electronic devices has been increased for over three decades in combination with technological innovations and business outcome. Lithography based micro manufacturing (LBMM) has remained the mainstream production technique to meet such demand. From the last two decades, non-lithography based meso/micro manufacturing (NLBMM) which are primarily material removal technologies are progressing well and the concept of micro factories have emerged [1-3]. Initial efforts were made using macro scale machine tools with micro-nano machining modules reaching feature size and accuracies in sub-micrometer range [4]. In the recent years, the technology has grown to a maturity level as micro machine tool development became a popular research interest. Many research groups and companies have developed these desktop machines claiming submicron level accuracies, despite the technical challenges in terms of low static and dynamic characteristics and requirement of very high spindle speeds in order to improve material removal rates [5]. Meso/micro part manufacturing of complex 3D shapes is successfully pursued using NLBMM techniques [6]. Micromachining can be defined in many different ways depending on the industry, feature size, and focus of interest. This paper focuses first to sketch a clear line between NLBMM and LBMM processes for meso/micro scale applications. For example, NLBMM are primarily material removal processes by geometrically defined cutting edges for the purpose of creation of precise three dimensional work pieces with dimensions in the range of a few tens of nanometers to some few millimeters [7]. In this definition of machining, the typical material removal processes are cutting, polishing and abrasive using different tool engagement methods as NLBMM is defined as mechanical cutting of features with tool engagement of less than 1 mm with geometrically defined cutting edges.

NLBMM covers a broad range of fabrication techniques for small scale parts and these micro manufacturing processes are combined to contribute towards microproduct development. Ultra-precision micro manufacturing methods are mostly comprised of the electrolytic in-line dressing (ELID) to produce smooth and curved surfaces, electro-chemical machining (ECM), die sinking electro discharge machining (EDM), wire cut electro discharge machining (WEDM) and laser micro machining (LMM) are employed at the meso scale for hard to cut materials and prototyping [8-10]. On the contrary, traditional machining processes like milling, turning, grinding, polishing and lapping have their limitations up to the micron level. According to the Taniguchi Accuracy graph modified by McKeown [11, 12], the machining accuracy limits of NLBMM processes have achieved 1 nm using present day ultra-precision machines (UPMs) [13, 14].

Micro components achieved using LBMM have also shown a remarkable progress. The critical dimensions of the component devices and features has been decreased from 15 μ m (first integrated circuit) to ≤ 45 nm [15], which is obtained by the next generation lithography (NGL). This is primarily considering two main factors: the feature size that is limited by the conventional optical mask process, and the cost which are expensive to operate, thus affecting the economy to make a reasonable profit through microelectronics industry. These processes generally include exposure, development, etching, sputtering, thermal removal processes, etc. Many of these chemical and thermal processes are used in the semiconductor industry and for micro-electro-mechanical-system (MEMS) related applications. This is referred as micromachining or LBMM with respect to this study and the feature size is considered ≥ 100 nm.

In LBMM, the basic feature size is defined by the wavelength of light used. Figure 1 shows the decrease in the exposure wavelength and the minimum feature size of largescale integration (LSI) devices over the years. The line representing the device miniaturization trend is steeper than the rate at which exposure wavelengths have been reduced. The current status of minimum feature size is presented in figure 1 [16, 17]. LBMM as the workhorse of the microelectronic industry, is subjected to the enhancement of the resolution for the smallest feature size. Furthermore, the post optical lithographical techniques, commonly known as NGL techniques are also important for finished products. Although several other contact based patterning techniques have been demonstrated such as nano-imprint lithography [18, 19], a shift by the microelectronic industry from the contact based techniques to non-contact techniques, such as x-ray, e-beam direct write, extreme ultraviolet (EUV), electron projection lithography, ion projection lithography (IPL) and focused ion beam, require the introduction of new tools, materials and process engineering technologies and research and development (R&D) costs.

3D printing at meso range has become a state-of-the-art technology. For the advancement in micrometer-scale, few interesting techniques have already been evolved from laboratories and moving towards industries, for example, direct laser writing and multi-photon absorption printing. These technologies are extremely important for optical industry to achieve the reliable fabrication of multi-level micro lenses [20]. On the contrary, the existing printing speeds are extremely slow to yield reasonable throughput at nanometer-scale. However, focused ion- or electron-beam deposition techniques exhibit 3D nanofabrication capabilities whereas the highest resolution for 3D patterning solutions are currently available by Scanning Probe techniques [21].

The purpose of this review is twofold. First, the identification of both processes with regards to the products/ applications and their features are highlighted including the



Figure 1. Comparison of the exposure wavelengths of various sources and the minimum feature size with timeline. Reprinted by permission from Springer Nature Customer Service Centre GmbH: [Springer Nature] [Nature] [16], (2000). Reproduced with permission from [17]. [Luong V 2018 Presentation EUV Lithography Coming to your local IC manufacturer! SoonTM, Arenberg, Youngster Seminar Leuven.]

third combined approach where the two techniques are merged as a process. Secondly, a comparison criterion is established in order to evaluate the application specific strengths and weaknesses of the two techniques followed by the future challenges that may influence the direction of development. As a result of comparison, a process effective guideline is developed that clearly highlights the application oriented LBMM and NLBMM characteristics.

2. Meso-scale manufacturing: an overview

Meso-scale manufacturing is reviewed using both techniques of LBMM and NLBMM. NLBMM largely involves the traditional manufacturing processes at meso scale that can form complex 3D geometries with a large variety in engineering materials. These processes are characterized by low to medium production rates, attainable high accuracies with miniature feature size and moderate level initial capital investment. The LBMM seems advantageous due to very high accuracies and production rates enabling the technology to keep the products cost low. However, LBMM needs large scale initial investment on fabrication facilities. Some details of the state-of-the-art manufacturing processes and the precision systems used for manufacturing of meso and micro scale components in both the approaches are given below.

2.1. Non-lithography based meso/micro scale manufacturing

NLBMM has variety of processes and machines at different scales. The list includes conventional processes like micro

milling, turning and drilling as well as ELID, ECM, EDM, WEDM, abrasive micro machining, LMM and 3D printing at the meso scale. Traditional micro machining processes were initially conducted through large scale machines [22–24], but proved uneconomical in terms of bulk material removal, large energy and space usage. In order to improve process efficiency, the micro machines were built for comparable work piece size and features. Some representative processes are explained for state-of-the-art micro/meso scale applications in table 1.

2.1.1. Micro machining. In this paper, NLBMM using small size machines are taken as examples as these machines are at the cutting edge in terms of economical micro feature development. Such machines have superiority in commercial prototyping at meso scale. NLBMM with desktop and standard size machines are reviewed in [4], in which classification is highlighted on the basis of machine foot-print size and the accuracies attained. The best example in terms of micro machine specifications is of FANUC's 'Robonano'. Though the machine foot-print size is large to maintain the high stiffness level, but the model is developed for micro manufacturing. ROBONANO α -0*iB* is a five axis computer numerical control (CNC) precision μ machining center. It is a multi-purpose machine used for milling, turning, grinding and shaping with a linear axis resolution of 1 nm. FANUC series 30i controller is applied for the CNC. Static air bearings are selected for the movement of slides, feed screws and direct drive motors. The machine has an overall size of $1500/1380/1500 \text{ mm}^3$ and the stroke length of $280 \times 150 \text{ mm}^2$ in the horizontal direction and 40 mm in the vertical direction. **Table 1.** NLBMM representative processes at Meso-scale. Reproduced from [25]. CC BY 4.0. Reproduced from [26]. CC BY 4.0.This [File:Wire erosion.png] image has been obtained by the author(s) from the Wikimedia website where it was made available[LaurensvanLieshout] under a CC BY-SA 3.0 licence. It is included within this article on that basis. It is attributed to [LaurensvanLieshout].This [File:Schematic representation of Fused Filament Fabrication 01.png] image has been obtained by the author(s) from the Wikimediawebsite where it was made available [KDS4444] under a CC BY-SA 4.0 licence. It is included within this article on that basis. It is attributed to [LaurensvanLieshout].attributed to [KDS4444]. Reproduced from [27]. CC BY 4.0.

	NLBMM		Process physics
Sr. No.	processes	Process sketch	Process for meso scale
1	µmilling/ µturning	Chip formation Depth of cut Work piece Work piece Tool Feed	Micro milling with standard size tools causes negative rake angle due to large tool edge size and small depth of cut and feed rate, resulting in rough surface of workpiece. Due to small workpiece size, distortions linked with residual and thermal stresses in workpiece remain signific- ant [28]. Very large spindle speed is required to maintain the cutting speed, due to small tool diameter. Tool deflection in smaller tools is a significant problem [29]. In micro turning, workpiece loses rigidity and deflect due to thin cross-section. This can be minimized by reducing thrust force of the tool [30].
2	μELID	Power supply Flectrolyte Brush(+) Electrolyte Electrolyte Coolant Work piece Feed	Electrolytic in-process dressing with metal bonded grinding wheels is used mostly for finishing optical surfaces, ceramics and metals. As brittle materials behave plastically at the nano meter scale, ductile-mode grinding is possible due to the formation of oxide layer on the grinding wheel surface. Uncut chip thickness is critical, as an increase in thick- ness can cause enough potential energy increase upon indentation to start cracking [25, 31].
3	μEDM	Electrode holder Power supply Dielectric tank Electrode tool Dielectric Workpiece	Micro EDM is suitable for efficient and burr-free, development of micro features, but the process is still not ideal for mass production. Small size tools and electrodes of less than 0.1 mm diameter are not available commercially. For very small electrodes, the tool wear significantly increases, when electric discharge capacities are slightly increased to enhance the process efficiency, but the micro feature quality is lowered. To maintain discharge energy, for micro EDM application, resistor capacity pulse generator is commonly used [26].
4	μ WEDM	Wire-Supply Wire Electrode Dielectric Fluid Workpiece Feed motion Spool	WEDM in the micro-meso scale is achieved, by use of thin copper wire of diameter of 50–250 μ m, that is used as the moving electrode. Dielectric fluid helps to flush the melted and evaporated workpiece material after each electrical discharge event. It is important to install a precision motion system for wire guidance and wire tension must be kept high in order to avoid deviated surfaces, tapering and undesired edges [32–34].
5	LMM	Laser Source Focusing Lens Workpiece Ablated material	Laser micromachining works with a laser source, reflecting and focus- ing optics. The most important factor is the timescale involved as con- tinuous wave, short and ultrashort. Ablation occurs and the size of the heat affected zone is associated with the time scale and the beam dia- meter of the laser pulse. The biggest zone emerges in continuous wave laser. Ablation with femtosecond laser with a beam diameter of as low as 1 μ m can give an accurate dimensional control for meso machining as compared to nanosecond and picosecond lasers [35, 36].
6	μ 3D printing	Extrusion Nozzle FDM 3D Printing	3D printing is an additive manufacturing technique that fabricates parts using four developed technology types namely stereolithography (SLA), powder bed fusion, fused deposition modeling (FDM) and inkjet printing. The earlier two methods use the laser, UV or electron beam source to initiate the resin reaction or material fusion. FDM use thermo- plastic based continuous polymer filament that is heated at the nozzle stage and the extruded material sits on the previously printed layer. Use of these methods for micro-meso manufacturing is growing fast and the product quality is highly linked with the method employed, resolution, surface finish and layer bonding. Present day SLA can

integrity [27, 37, 38].

make micro features of size 10 μ m with good accuracy and structural

Table 2. Meso scale artefacts using NLBMM techniques. Reproduced with permission from [39]. [KERN Microtechnik GmbH source]. Reproduced with permission from [40]. [© BMF Boston Micro Fabrication]. Reproduced from [41]. CC BY 4.0.

Sr. No.		Example	Process/material	Feature size	Machining time/ accuracy/ resolution
1	Test membrane for computer chip manufacturing (Courtesy of KERN Microtechnik	60 times magnification	Drilling of large number of holes/Macor	Dia. 130 μm	7.8 s for each hole/ $\pm 2 \ \mu m$
2	Micro turbine wheel for high-speed micro fluidic pumps (Courtesy of KERN Microtechnik GMBH) [39]		five-axis machining/high performance polyimide based polymer (Vespel)	Dia. 0.7 mm	_
3	Test membrane for electronic chips manufacturing (Courtesy of KERN Microtechnik GMBH) [30]		Drilling of 648 holes from both sides/Vespel	Thickness: 0.5 mm Drill dia.: 60 μm	Total machining time $<20 \text{ min/}\pm 2 \mu \text{m}$
4	Medical device— Endoscope shell (Courtesy of Boston Micro		Micro-precision 3D printing utilizing projection micro	$9.8 \text{ mm} \times 9.8 \text{ mm} \times$ 13.8 mm Tube diameter = 1.2 mm, min. wall this/mass	Tolerance = ± 0.025 mm Resolution: 10 μ m
5	1 mm long gradient chain-mail [41]. Smooth surface with features that range from μ m to hundreds of μ m	1 mm Single working field (125 µm) 250 µm	3D laser lithography or multiphoton stereo- lithography	Internal radius of the largest ring: $100 \ \mu m$ smallest ring radius: $5 \ \mu m$	Total fabrication time: 26 min/Step size for slicing and hatching: $0.3 \ \mu m$
6	3D Integrated microelectronic subsystems (Courtesy of Boston Micro Fabrication) [40]		Projection micro stereolithography ($P\mu$ SL). Low-viscosity ceramic metallized to allow conductive connections.	Curved routing via hole diameter: 10 µm Pitch: 20 µm	Printing resolution: 2 μ m
7	Hard milled mold insert (Courtesy of KERN Microtechnik GMBH) [39]		M340 mold steel Hardness: 56 HRC	Groove width: 0.2 mm Groove depth: 0.6 mm	Cycle time: 30 h Smallest end mill: Ball Ø 0.2

Surface roughness of Ra 1 nm is achieved in the turning operation on aspherical lens core of material Ni-P plate. Table 2 shows some meso scale manufacturing examples using materials like ceramics and metallic alloys for getting complex 3D shapes. These examples show the state-of-the-art NLBMM capabilities in terms of variety of shapes in 3D at meso scale. Some state-of-the-art micro machines and the specifications are shown in table 3. Table 3 is showing the comparison of the capabilities and design aspects of current state of the art micro machines. There are machining centers, milling and turning machines and a hybrid machine capable of micro EDM, WEDM, ECM and ELID grinding. Micro milling and other machines made by the AIST, Japan are the smallest in size and weight. Robonano machining center has the highest resolution achieved as compared to other machines. Robonano has also achieved the

Machines	Make/overall size dimensions $L \times W \times H (mm^3)$	Designed for micro machining processes	Maximum spindle speed	Smallest work piece dimensions/accuracy achieved	Positioning accuracy/resolution
MTS5/MTS6 (Micro milling)	Nano Corporation, Japan [42]/260 \times 324 \times 370	Milling	20 000 rpm	$50 \times 50 \times 16 \text{ mm}^3/\text{sub-}$ micron surface roughness achieved	$\pm 1~\mu$ m/0.1 μ m
Micro turning/milling	AIST, Japan [2] $32 \times 25 \times 30.5$ (Lathe)	Turning/surface cutting, drilling	10 000 rpm/ 20 000 rpm	Ø2 mm/4 \times 4 mm ² Surface roughness: 1.5 μ m, Roundness: 2.5 μ m	$\pm 0.5~\mu$ m/0.05 μ m
ROBONANO α - $0iB$	FANUC, Japan [13] 1500 × 1380 × 1500 Travel X/Y/Z 280 × 150 × 40	Milling, turning, grinding and shaping	70 000 rpm	Surface roughness: R_a 1 nm is achieved while turning aspherical lens core	0.001 μ m (resolution)
MMT—Micro	KERN Germany [39] 3110 × 1510 × 2965 Travel X/Y/Z 350 × 220 × 250	Milling, drilling	50 000 rpm	Ø350, H: 200 mm/ ±2.5 μm	$\pm 1~\mu$ m/0.1 μ m
DT-110	Mikrotools, Singapore [43] 3000 × 2000 Travel X/Y/Z 200 × 100 × 100	Turning, milling, EDM, WEDM	5000 rpm	Silicon grinding: Surface roughness: <i>R_a</i> 3 nm	$\pm 1~\mu$ m/0.1 μ m
AGIETRON MICRO NANO	Agiecharmilles, Switzerland [44] Travel X/Y/Z Micro module: $220 \times 160 \times 100$ Nano module: $6 \times 6 \times 4$	Die sinking EDM		Surface roughness Micro module: R_a 0.1 μ m Nano module: R_a 0.05 μ m	Micro module: $\pm 1 \ \mu$ m/0.1 μ m Nano module: $\pm 0.1 \ \mu$ m/0.02 μ m

Table 3. Comparison of micro cutting machines (NLBMM): features and capabilities.

highest work piece quality with a surface roughness of 1 nm. MMT from KERN, Germany and Robonano has the highest spindle rotation speeds reaching 70 000 rpm. MTS series from Nano corporation, Japan has developed many micro lathes and milling machines. The micro lathes are capable of machining submicron level circularities and work piece surface roughness. Micro machines shown in figure 2 are some state-ofthe-art developments in the NLBMM cutting processes and major examples are developed by the commercial companies. Figure 2(d) is showing an example of a three-axis CNC micro machine using a nature inspired machine frame design for high structural stiffness with a conical egg-shaped cut in granite machine frame. A similar example is of KERN Pyramid Nano [45] where submicron accuracy is achieved through five serial axis attached with a pyramid structure and hydrostatic bearings.

2.1.2. Micro EDM. Other micro machining processes like ELID, ECM, EDM, WEDM, abrasive micro machining, LMM [46, 47] and micromolding can also be included for micro features development. DT-110 developed by Mikrotools, Singapore has capabilities of variety of ELID and EDM processes that has produced surface on silicon with Ra value of 3 nm. It is shown that the ECM has also been used in producing micro features on hard surfaces and features as small as $0.5 \,\mu$ m

are developed [48, 49]. Figure 2(e) shows 'Agietron Micro-Nano' die sinking machine that can perform micro drilling to machining of micro-structures with the addition of nano module that can fit on the same machine by replacing the rotary axis of the AGIETRON micro. The nano module is highly agile and uses voice coil linear motors and parallel kinematics for axes movements.

2.1.3. Micro machining through abrasives and lasers.

Abrasive micro machining is also explored to develop micro features. The technique is successfully used in the microfluidic channels machining [53, 54]. Liu [55] developed a high pressure abrasive slurry jet micro machining equipment and found it a viable technology for producing concave and convex surfaces of optical lenses, with low roughness in variety of materials. Micro machining using lasers or LMM is also in use for industrial micro-engineering applications with different techniques like direct-write LMM [56], CO2 gas laser LMM [57] and excimer laser LMM [58, 59]. Variety of materials can be used to produce micro features with submicron tolerance range using high intensity short laser pulses. Micro molding [60] of plastics also involves micro feature creation like wall thickness up to 80 μ m is achievable utilizing high performance plastics and maintaining tolerance of $\pm 5 \ \mu m$.



KERN, Germany (courtesy of KERN Microtechnik GMBH), (d) micro milling developed in University of Manchester, UK [52], (e) 'AGIETRON MICRO NANO', nano module (courtesy of Agiecharmilles). Reproduced from [50]. CC BY 4.0. Reproduced with permission from [51]. Reproduced with permission from [39]. [KERN Microtechnik GmbH source]. [52] Ogedengbe TI 2010 A Contribution to the Design and Operation of a Micro Milling Machine, PhD Thesis, University of Manchester, UK. Reproduced with permission from [44].

2.1.4. Micro 3D printing. There are optical 3D printing [61] and laser 3D printing [62] additive manufacturing techniques for microfluidics and medicine applications at meso scale as 3D printing currently, is enabling multiple scale features to co-exist on a single artefact [41, 63–65]. FDM are popular 3D printing machines for low cost and high-speed rapid prototyping. However, workable materials are only thermoplastics, that are extruded to form layer over previously settled layer. The finished product has relatively weak mechanical properties with minimum feature resolution range from 50–200 μ m [66]. Powder bed fusion is commonly known as selective laser sintering and selective laser melting are fine resolution and high-quality printing in which compacted fine metallic powders are fused using laser scanning. Metals, alloys and some polymers

are used in this slow and expansive method. Meso scale applications are employed in biomedical implants, electronics and aerospace with minimum size feature resolution in the range of 80–250 μ m [37]. Inkjet printing has made it possible to make large concrete structures using concrete pastes and crafting contours. Ceramics and soil are also in use for such coarse and layered based structural applications. In biomedical implants, inkjet printing has been used with minimum feature resolution in the range of 5–200 μ m [37]. μ Stereolithography printing has the finest resolution available in the range of 10 μ m. The process is limited to polymers that are photo active monomers resins. High quality expansive biomedical, electronics and soft robotics related products are printed at a slow rate [66, 67].

2.2. Lithography based meso-micro scale manufacturing

There are different types of LBMM manufacturing processes. LBMM approach patterns the material based on the desired design through either top-down (i.e. surface micromachining) or bottom-up (i.e. bulk micromachining). This approach generally involves lithography that transfers the design onto the material and etching technique that removes any unwanted materials to realize the design. Bulk micromachining is restricted by the substrate which is commonly silicon. The mechanical properties of final components are strongly dependent on the properties of silicon. In contrast, surface micromachining patterns materials that are deposited on top of the substrate (e.g. silicon) and the mechanical properties of final components varies depending on the types of materials that are deposited, such as metals through sputtering and oxides through chemical vapor deposition (CVD).

Lithography is the process by which the patterns are realized in a chemically resistant polymer (i.e. resist) applied by a spin coater onto a substrate [68]. The thickness of resist is dependent on the spinning speed and the viscosity of resist itself. In optical lithography process, the resist is exposed to UV source through a quartz mask with an opaque patterned chrome layer to either break or link the polymer chain. The former is called positive resist (e.g. AZ9245) and the latter is negative resist (e.g. SU-8). After UV exposure, the soluble resist is removed in a development process and the remaining resist is baked in an oven to further harden the chemical links. In contrast, non-optical lithography techniques direct write patterns on to the resist using an energetic beam of electrons/ions across the wafer.

Figure 3 illustrates a standard optical lithography process involving selective removal by selectively etching unprotected materials from the substrate to reveal patterns. After the resist is hardened, uncovered material is then removed by an etching process where the etchants could be either wet or dry. Wet etching is commonly used to remove silicon dioxide, silicon nitride, and the material is removed either in an isotropic or anisotropic manner. Dry etching is achieved using plasma at low pressure and it is a combination of chemical and physical removal. The physical removal process is extremally important in LBMM as it provides anisotropic etch profile with high aspect ratio (e.g. >40:1) in components. Table 4 shows the comparisons of commonly used lithography techniques.

2.2.1. Optical lithography. In optical lithography, patterns are created on the resist materials coated on the substrate after the exposure of UV light through a mask and subsequent development processes. Table 5(a) shows Scanning Electron Microscope (SEM) image of a MEMS structure fabricated by optical lithography. The resolution limit of optical lithography is determined from the Rayleigh equation. The resolution limit *R* and depth of focus (DOF) of a lithographic system are given by the following equations [75]:



Figure 3. Photolithography process steps: (a) subtractive cleaning, (b) photoresist deposition, (c) UV exposure, (d) post baking, (e) development, (f) metal thin film deposition, and (g) polishing and etching. Reproduced from [69]. CC BY 4.0.

$$R = k_1 \frac{\lambda}{\text{NA}} \tag{1}$$

$$\text{DOF} = k_2 \frac{\lambda}{\left(\text{NA}\right)^2} \tag{2}$$

where λ is exposure wavelength, NA is numerical aperture of optical system, k_1 and k_2 are constants that depends on the resist material, process technology and employed exposure technique. For the high resolution, a shorter wavelength and higher NA optical systems and resist resolution are used. The minimum feature size that could be achieved is comparable or slightly smaller than the wavelength of optical system which needs a high NA ≥ 0.5 . However, a high NA optical system limits DOF which results in making the exposure process more sensitive to the thickness and absolute position of the resist layer. Thus, leading to the focused beam diverged more rapidly from the focal point [76].

Conventionally, resolution improvements for IC fabrication processes have been achieved by a decrease in printing wavelength i.e. from G-line at 436 nm to I-line at 365 nm as shown in figure 1. Such illumination systems used multispectral lines filtered mercury arc lamp sources. However, an improvement in radiation sources was carried out by excimer lasers at 248 nm and 193 nm with introduction of KrF and ArF, respectively. Moreover, figure 1 shows that progress in minimum feature size is on a much steeper slope to that of lithographic wavelength. With the introduction of 180 nm technology during 1999, significant feature sizes below 248 nm wavelength were achievable [77]. To attain feature sizes less than the wavelength of the exposure system, improvements in imaging resist materials are attributable. The modern resist materials exhibit high imaging contrast and even light intensity is less than full modulation of small features. A combination of

Technique	Mini. feature size	Fabrication area	Fabrication time	Cost	Throughput	Applications
Photolithography (contact & proximity printings) [70]	2–3 µm	Large	Short	High	Very high	Research and production of MEMS devices.
Photolithography (projection printing) [71]	A few tens of nanometers	Large	Short	High	Very high	Research and production of MEMS devices.
Electron beam Lithography [68]	<5 nm	Small	Long	High	Very slow (e.g. 8 h to write a chip pattern)	Mask and IC production.
Ion beam lithography [72]	$\sim 20 \text{ nm}$	Small	Long	High	Very slow	Patterning in R&D including hole arrays and plasmonic lens.
X-ray lithography [73]	$\sim \! 20 \text{ nm}$	Large	Short	High	High	Research and development.
Extreme UV lithography [74]	<50 nm	Large	Short	High	High	Research and development.

Table 4. Summary comparison between different lithography techniques.

Table 5. Artifacts summary using different LBMM techniques. Reprinted from [82], Copyright (2015), with permission from Elsevier. Reproduced from [79]. CC BY 3.0. Reprinted from [83], Copyright (2012), with permission from Elsevier. Reprinted from [84], Copyright (2012), with permission from Elsevier.

Sr. No.	Techniques	Artifact examples	Explanation
1	Optical lithography		SEM image of a MEMS structure fabric- ated by optical lithography.
2	Electron beam lithography		Development of HSQ dense parallel lines using lithography at different developing temperatures. 100 nm (a and b), 30 nm (c and d) line-width and 100 nm pitch [82].
3	Ion projection lithography (IPL)		SEM image of Ag nano disks fabricated by ion beam lithography [68].
4	Proximity x-ray lithography		Examples of structures fabricated using proximity x-ray lithography [83].
5	Extreme ultraviolet lithography (EUV)	60nm	CD-SEM, cross section images of 32 nm half pitch resist lines/spaces structure after lithographic exposure [84].

resist material imaging contrast and process control can reliably achieve subwavelength features and consequently reduce the value of k_1 .

2.2.2. Electron beam lithography (EBL). EBL use a fine focused electron beam that has the capability of extremely high resolution with a large DOF. It is used to fabricate the masks and reticules for optical lithography. Owing to its high-resolution, it is used for fine scale devices for fundamental and device verification and high operating frequency devices [78]. The largest problem with EBL system is its low throughput due to slow scanning of electron on the surface and inability to employ for the mass-produced LSI circuitry.

There has been a considerable interest to increase the throughput of EBL by enlarging and shaping the electron beam, for example to vary the size and shape of electron beam during writing process. The efforts have put-forward to ensure writing time insensitive to the minimum feature size i.e. coarser features can be written with a larger beam during a single pass. Furthermore, several areas of the pattern need to be exposed simultaneously [76]. Table 5(b) shows scanning electron microscopic image of electron beam direct write on UVIII resist to achieve chiral structures.

2.2.3. Ion Projection Lithography. In IPL, the electron beam is simply replaced by an accelerated ion beam to directly punch a metallic film on the substrate, as a result of the heavy mass of ions compared to that of electrons. Due to much high mass, the beam is less prone to distortions owing to backscattering from the substrate and results to improve the imaging capabilities of the lithography system. The resolution of ion beam lithography techniques is of the order of 5-20 nm due to ultra-short wavelengths of electron/ion beams in the order of a few nanometers. The lack of throughput limits their applications within research and mask fabrication. However, the highresolution ion beam systems are in a primitive state of development compared to electron beam systems. Table 5(c) shows an example of silver nano disks array fabricated on a glass substrate by ion beam lithography [79].

Comparing with optical 2.2.4. Proximity x-ray lithography. wave, x-ray penetrates the vast majority of materials except those with much higher atomic numbers and there is no refraction after x-ray enters the materials. The x-ray exposure can only be 1:1 with a proximity gap between mask and resist [80]. In the proximity lithography, the mask is placed in close proximity to the substrate and the pattern is produced by the shadow of the mask on the semiconductor substrate during exposure. In a proximity x-ray system, the x-rays are first collimated using a mirror of silicon carbide and then allowed to pass through a transparent window of beryllium into a chamber containing the mask and the semiconductor substrate. The mask is usually produced on a membrane of low atomic number materials (e.g. silicon carbide) which are transparent to x-ray, while materials with higher atomic numbers (e.g. Au and W) can effectively block x-ray such that the patterns are generated by patterning those high atomic number materials. Table 5(d) shows examples, fabricated using proximity x-ray lithography with critical dimensions between 100 nm and 150 nm [81]. Although the proximity x-ray lithography is a good candidate for NGL process in LSI, there are still lots of challenges that need to be overcome, such as precise gap control between mask and resist.

2.2.5. EUV lithography. EUV lithography is used to produce extremely small pattern of ≤45 nm and below. EUV lithography uses the exposure wavelength of 13.5 nm and photons that are obtained from plasma source. The technique is based upon the similar principle as the conventional optical projection lithography and obeys Rayleigh equations for system resolution. At such a small wavelength region, the absorption of light is very strong that cannot makes the use of refractive optics and instead, employs all the reflective optics [85]. Furthermore, in all reflective optics, the conventional mirror surfaces cannot be used. Therefore, one must use the multilayer structures that rely on interference principle to show a reasonable reflectivity. However, the obtained reflectivity is around 60%-70% at these wavelengths. Table 5(e) shows dense patterns of tilted cross-section SEM images after Cr and W etching by EUV lithography [86].

The improvements in lithographic resolution and edge contrast were achieved with improvements in exposure tools (projection lens), decrease in exposure wavelengths and photoresists which results in projection photolithography. In this projection system, the lens is used to focus the mask patterns to smaller areas. Therefore, state-of-the-art current projection systems can achieve resolutions down to a few tens of nanometers [71]. Moreover, projection lithography is aligned with complex systems which are widely less available and are not cost-effective solutions in comparison to contact and projection photolithography.

2.3. Meso/micro scale manufacturing using combined approach

A new approach targeting meso/micro-scale manufacturing is to develop micro artefacts by employing NLBMM and LBMM techniques in a simultaneous way. The meso scale fills the gap from sub-10 μ m to near 300 μ m features [87]. Meso scale products can take advantage in such that the features produced from one technique can be finished using the other technique. This can be considered as a combined approach that can fall within the range from sub-micron to the meso scale. Below 10 μ m manufacturing regime covers the semiconductor, and other nano-manufacturing processes like direct writing techniques through laser and other additive manufacturing processes [88] and fabrication in micro and nanomanufacturing. On the other side, high precision NLBMM are employed beyond 300 μ m manufacturing regime. There are a mix of approaches which can cover the gap areas and are termed as combined approach in this work as shown in figure 4.



Figure 4. NLBMM, LBMM and combined micro fabrication specific zones.

Meso scale regime is a buffer region where the characteristic features from the bordering scales can be employed. There are examples of combining LBMM and micro EDM from NLBMM to fabricate microstructure in tungsten carbide for micro tools and other micro features involving high aspect ratio [89]. Fabrication of soft polymers using photolithography presents a potential area for combined manufacturing approach in which lab-on-chip devices are fabricated for medical applications. These are popular products for biologists to discover new drugs, clinical assessments, cytometry and optimal dosage experimentation. Lab-on-chip microfluidic device contains microchannels for functions of mixing, filtering and analysis. Silicon or glass substrates are commonly used to produce fluidic chips by deposition of metallic layers and subsequent photolithography for pattering of layers to outline microchannels. The process is completed by etching to reveal desired structure. Other alternative is to do micro milling of the metallized substrate to reveal electrodes [90]. Some examples of combined approach in electronic industry include LMM of polymer substrate, micro drilling of holes, patterning and scribing in lab on chip devices and wafer substrates, micro features fabrication in MEMS and ultrasonic machining for semiconductor component slicing and trimming. Other example includes the bespoke patterned micro tools fabricated through lithography are used in die sinking electro chemical machining for manufacturing of complex profiles [89–91].

There is a potential for some LBMM and NLBMM approaches that can be combined to form meso-scale 3D features. In this regard, LBMM consists of processes typical to semi-conductor processing in which, for example, a film is deposited via vapor deposition techniques followed by chemical or reactive ion etching. For example, bulk micromachining, surface micro machining and direct ceramic machining with the support from WEDM has the potential for 3D meso-scale manufacturing having capability of handling multiple materials [92]. The applications include surgical instruments on the meso scale like cardiovascular stents, lab on chip devices and micro needles that can be fabricated using LBMM and further/alternative processing can be done through micro wire EDM, LMM and electroforming, micro ultra-sonic machining (MUSM) and micro-ECM. MUSM is also used as a functional device where the ultrasonic cutting tool actuated by piezoelectric actuator for the cutter to resonate [93] and cut through tissues like hardened lenses with cataracts.

In most of the examples considered, NLBMM is used either as support/finishing process or identified as an alternative method to produce 2D/3D micro artifacts. Other examples are complex 3D shapes, such as V-grooves, channels, pyramidal pits, membranes, vias, and nozzles are formed through bulk micro machining [94]. In bulk micromachining, the substrate material, which is typically single-crystal silicon, is patterned and shaped to form an important functional component of the resulting device. There are ways to form micro channels using cutting plotter blades to develop lab-on-chip device for blood sampling and analysis [95]. Micro needles are developed with different materials like in stainless steel [96] using femtosecond LMM for drug delivery to diabetic rats. Other manufacturing methods are employed for polymer micro needles using bulk lithography, droplet borne air blowing and injection molding [97, 98]. These examples are discussed as the potential manufacturing process options to be used for same type of products. As a fully developed combined approach, ECM is integrated with dry etching of photoresist to reduce the size of tip opening. The gold dot patterns are then produced after lithography with a dimeter of 200 nm [99].

Stereolithography based 3D printing [100] is another approach gaining popularity for tissue engineering and developing bio materials at different size scales. The technique combines the flexibility of 3D printing with a laser light source to cure liquid resin into hardened form, thereby, avoiding pattern and mold requirements, an effective way to make cavities and freestanding structures. In order to further improve the structural properties and making the parts functional (electrical conductivity), SLA printed parts are metallized through sputtering/CVD and further chemically etched [101, 102]. The process can be applied to different types of polymers, that enables metallization of polymer parts, making easier to manufacture printed circuitry. The etching provides uniform coverage of metal coating, even on hard to access zones of the complicated, small size, 3D parts. Overall, this has developed into an important meso scale application in which CVD and etching are followed, once the part is printed using SLA, making it a truly combined approach.

3. Comparative analysis

While looking at the NLBMM, LBMM and the combined approaches, it seems obvious that there are specific size scales and other associated issues that can be identified for a particular approach. As discussed, most NLBMM techniques are downscaled in tabletop size machines that can manufacture features in micron scale with higher accuracies in an energy efficient way. The LBMM techniques were established to fabricate micron size devices and features and now the feature resolution has reached to the nano scale. A comparative study is conducted to compare the effectiveness of each approach. The feature size, capability to manufacture variety of shapes, use of various engineering materials, production rates, attainable accuracies and required investments are some of the important factors to be included in comparison. Table 6 shows the comparison of the three approaches. The comparison table shows that NLBMM processes have a dominant role at micron scale. In contrast, modern day LBMM techniques are mostly utilized for achieving nano scale resolution as required by the semiconductor industry.

As getting the right size, tolerances and shape is important for meso scale features, therefore, many overlapping multiscale manufacturing options are studied and compared. The criteria developed for the comparison of the three techniques is focused for the meso-scale features and products normally used in application of medical devices, watch and electronics industry. NLBMM processes are suitable for development of two and three-dimensional intricate parts having micron size features in traditional materials. As a concept, NLBMM processes employ subtractive machining or material removal technologies except 3D printing for meso-scale products and features. Subtractive NLBMM processes have the potential of expanding the manufacturability of meso-scale components and complement LBMM and additive technologies. Examples of medical devices like micro-needles are already discussed in the combined approach section.

As far the achievable accuracies are concerned, both the techniques are comparable attaining nm level surface roughness and accuracies. Most of the NLBMM processes are suitable for batch manufacturing, hence, low to medium level production of meso-scale artifacts is viable, however, the production rates are heavily dependent on the feature complexity. As an example, the machining time for any drilled hole in micro artifact shown in table 2 (example 1) is 7.8 s. On the other hand, the established products using LBMM can be mass produced at a very high rate. For the comparison of initial capital investment and operational costs, it is relatively cheaper in case of NLBMM to establish a new production line. Another feature is the process re-configurability in NLBMM as multiple micro machines can be re-configured to produce small batch production. Batch production in lithography-based device manufacturing is common that is based on the development of specific tooling and the cost variation depends on the application. In LBMM, short wavelength optical lithography and the use of new materials including biomaterials are the new trends. In NLBMM, machine tool designers are employing innovative mechanisms like parallel manipulators, machine re-configuration, sequential micro machining [121] using a single machine tool and intelligent machine systems.

4. Challenges for NLBMM and LBMM

At the meso-scale, both the LBMM and NLBMM seems to be viable options for various types of applications. However, there are number of challenges in both the techniques that are needed to overcome. The challenges include development of new products at the meso-scale, their design and materials involved relevant to the production process, metrology techniques, packaging, contamination, assembly and selfassembly in addition to modeling and scaling laws at mesoscale, to name a few. The factors are discussed in detail for both the cases with a view of improvement in processes in future.

4.1. Challenges for NLBMM

As NLBMM is a developing technology in the domain of micro/meso scale manufacturing. The issues for the costeffective implementation of NLBMM need to address the following concerns.

4.1.1. Ultra-precision machinery. The high-end UPMs are designed with features having tight specifications in terms of friction less drives, moving parts with extremely high resolution, repeatability and position stability of dynamic system. The biggest challenge is the cost effectiveness of the manufacturing process using such machinery for meso-scale components that are manufactured for applications like microfluidics, photonics, energy harvesting and miniature devices. High resolution components in both linear and rotary stages

Process characteristics	NLBMM	LBMM	Combined approach
Processes	μ ECM, μ EDM, μ WEDM, μ USM, μ milling, μ turning, LMM, μ molding, abrasive μ machining.	X-ray, e-beam direct write (EBDW), extreme UV (EUV), electron projection (EPL) and ion projection lithography (IPL) [78].	Bulk micro machining with WEDM, LMM and micro drilling, cutting [103]. SLA with CVD and chemical etching.
Applications only in meso scale	Watch industry, medical devices, sensors, micro actuators, micro pumps,	Medical devices, micro actuators/sensors, micro electronics.	Surgical devices, lab-on-chip devices, micro-needles [104].
Minimum feature size	Meso-scale (few microns to few mm).	Up to 50 nm for most of the semi-conductor industry. Both micro and nano scales are commonly achievable [77].	Employed at micro meso scale (see figure 4). 10 μ m size features are possible with SLA that can be further processed to make functional
Feature shapes	Complex 3D shapes are commonly manufactured at meso micro scale.	2D, 2.5D up to 3D geometries with slender, hollow and free-standing structures [106], but 3D capabilities are limited.	parts [102, 105]. 3D is possible depending upon the selection of major process. Most common with SLA 3D printing.
Process materials	Almost all engineering materials used in large scale manufacturing can be processed at meso scale.	Silicon, metals, oxides, semi-conductors and hydrogels [107].	Variety of engineering materials including polymers, metals and ceramics.
Production rates for meso scale manufacturing	Low to medium scale production is possible. Mainly depends on machining time,	Mostly mass production processes.	Application specific. Low to medium where major portion of the process includes NLBMM or
Feature accuracy at meso scale	feed rate, speed etc [108] $\pm 1 \ \mu m - \pm 2.5 \ \mu m$ in meso scale manufacturing. Further accuracy range is achievable using ultra precision machinery [109]	±1 μm–±100 μm [110].	stereolithography. $\pm 10 \ \mu\text{m} - \pm 50 \ \mu\text{m}$, using stereolithography based 3D printing technology [111].
Process resolution	$0.02 \ \mu \text{m} - 0.1 \ \mu \text{m} \ [44].$	0.1 μm–1 μm [68].	For different types of stereolithography: 10 μ m–
Process initial investment	Price for high precision CNC micro machine tool can range from 40k–70k USD [52]. Mainly depends on the required precision. Large size machines can cost more	Capital investment for lithography based fabrication equipment \$20 million–\$100 million [68, 113].	SLA printers costs from \$5k-\$15k. No extra investment required in case LBMM and NLBMM process equipment are installed.
Tooling/consumables cost	Cheap consumable tools e.g. micro end mill cutters are available from $80-$ $1000 \ \mu m$, [50]	Costly molds and tools specific to the feature size. Consumables cost can reach upto 2^{-3} million yr ⁻¹ . [114]	In stereolithography 3D printing, material and tooling can cost up to \$30–\$40 per hour of print [115].
Operational costs	Energy, labor and other overheads for three axis CNC machine operational cost: \$35–\$40 per hour [24, 116].	\$50k-\$500k per mask. Mask utility is based on the number of exposures per mask [114].	Using stereolithography 3D printing, energy, labour and overheads can cost up to \$50–\$60 per hour of print [115].
Process re-configurability	Process re-configuration in CNC machining centers for batch production.	Costly tooling specific to the feature or device. Phase-change material photomasks are employed to optically reconfigure mask pattern on demand [117].	Using SLA 3D printing, multi material process reconfigurability is possible [118].
Functionally active parts manufacturing	NLBMM processes are known for manufacturing of passive parts. However, shape-memory alloys are made by casting.	LBMM has limited capability to produce active parts using shape memory materials [119].	Stimulus responsive shape memory polymers create functionally deployable, lightweight metamaterials using 4D printing approach [120].

Table 6. Comparison of three approaches for meso-scale manufacturing.

are a must requirement for NLBMM production equipment. Actuation components including high torque motors in small packaging and high-resolution encoders that can resolve 1 nm are required in moderate price range for production and economic manufacturing of meso-scale parts, products and features. It is also important that for a fixed control memory bit, a small machine's stage can have a better spatial resolution than the large machine axis [7]. For precision mechanics, the micro stages are designed with unconventional designs using parallel kinematics [122], flexures [123], serial-parallel hybrid axis [4, 124] and using shape memory alloy [125], though not commercialized on a mass scale.

It is expected that the demand for 4.1.2. Micro components. meso-scale 3D components and features will increase in various industries from electronics to biomedical. Precision micro stages, micro spindles, motors in small packaging, micro actuators, micro tools, small scale fixtures and handling devices are the key components in NLBMM production machinery. Software technologies include machine tool components with suitable control algorithms as well as an understanding of process physics is needed. As an example, ultra-precision positioning systems with 1 nm positional resolution are developed by Otsuka et al [126]. A magnetic bearing based stage of 0.1 nm resolution is developed by Holmes et al [127]. A 25 pm positioning resolution system is developed by Mizumoto et al [128, 129] using twist roller drive and aerostatic guide way. Friction roller drive is invented by keeping the drive roller at a very small angle to the driven roller. Vacuum chucks are proposed by Qiao and Bu [130] for handling of micro parts. Micromachining requires very high-speed spindle speeds due to small tool diameters that can cause large centrifugal force during spindle rotation, can create massive radial loading conditions for precision bearings. For micro actuators and stages, use of piezoelectric actuators are the choice in high precision micro stages in addition to the precision mechanisms.

4.1.3. Micro factory. NLBMM productivity can be enhanced by developing micro factories [2, 24, 131] that consists of high precision micro machines and associated equipment. Associated equipment also includes the working environment in which the micro machines work, e.g. a desktop clean room, a centralized control system and other modules are developed [132–134]. However, the biggest challenge lies in the fabrication of the proper tool geometry for creating various 3D features. The other issue is the micro factory compatibility to accommodate multi-scale components for assembly processes.

4.1.4. Multi-scale physics. Physics at micro/meso scale has different effects as compared to the macro scale. The fundamental difference lies in the influential surface forces as compared to the smaller inertial forces [24, 135, 136]. This results in the development of many handling, inspection and manufacturing devices at a small scale. The micro machined products cannot be reliably produced without sensor-based metrology and measurement techniques. Due to the small

scale of products, it is necessary to use non-contact measurement [137] techniques for precision quality products. This will reduce the damage to parts and improve inspection rate to enhance productivity. Fabrication of smaller features with reliability at high tolerance also requires visual and in-process inspection techniques [137, 138] of micro parts. The additional challenge in such products is the assembly of multi scale parts as this type of assembly needs special fixtures and tools.

4.1.5. Sensors. Conventional manufacturing machines utilize a lot of sensors which cannot be effectively used due to practical considerations, if meso scale parts are produced using high precision micro machines. The sensors can be divided into three applications areas in micro-meso scale manufacturing. These include sensors used in CNC machine operation, sensors for metrology and in-process inspection and sensors employed for condition monitoring and health assessment of manufacturing machines. Large size sensors like limit switches, encoders, read-heads, linear scales and other transducers cannot work on high precision small scale machine. To cater for micro machines, small size, high resolution, high precision and reliable sensors need to be selected.

Micro machine and micro artefact metrology for measuring micro features is another challenging area. The main technical issues are artefact/feature damage due to contact and micro feature size smaller than the measuring probe itself. Non-contact vision based [137, 138] techniques are in development to cater for faster measurements. These devices in addition to other such non-contact sensors like ultrasonic, LIDAR and radar-based sensors connected through IoT are a necessity if large amount of data has to be collected and processed. Another application area is emerged with the development of micro metrology devices [139], micro probes and even complete micro coordinate measuring machine (CMM) systems. E.g. a micro CMM is developed with a resolution of 1.3 nm [140]. Micro probes are another necessity in micro feature metrology, in fact one of the two effective solutions. The solution is either the development of micro probes and tactile sensors smaller than the size of the features or a complete non-contact metrology system that can extract the features with high accuracy from the image. Non-contact ultrasonic and acoustic emission-based sensors are also in use in such applications [141].

In today's new manufacturing paradigm of IoT enabled production systems, micro machines need to be integrated on network and ultimately to the cloud for smart manufacturing of micro products. In-process inspection of micro tools and micro artefacts/features and condition monitoring of machines can generate large data sets that can become a big data problem to predict better maintenance schedules of micro machines and micro factories.

4.1.6. Micro tools. NLBMM needs all types of micro tools to run the processes on smaller scales, but there are typical issues involved. First to achieve a micro tool geometry is a challenging task for diameters of less than 50 μ m. Simple geometries in less than 50 μ m diameter are available in drill

sets [7], but milling cutters in these sizes are still not commercially available. Even, if the complicated tools are fabricated to cut 3D micro features, the micro tool working environment needs to be controlled very strictly in order to avoid tool breakages. Micro tools have limited use when cutting hard to cut materials. Cuts with large speeds and feeds are generally not possible, however, improved chip removal can result in better finish [142]. A micro ball-end mill [143] is designed to machine gold using 5 axis machining as an example of improved chip removal. Thermal stresses can be fatal in the micro tool as fast heating and cooling takes place due to small cross-section sizes. Effective cooling mechanisms, in-process inspection and condition monitoring of micro tools [144] are in infancy stage of research.

4.2. LBMM issues and challenges

Lithography is a key microfabrication technology as it determines the dimension, quality and quantity of the device. Miniaturization is a drive-in recent development and commercialization such that many components (e.g. Sensors, CPUs) are getting smaller and smaller. As the feature size decreases based on the Moore's law, fabricating small features become increasingly difficult as well as the cost and functionality of the fabrication process. The requirements of microfabricated devices are reliability, low power dissipation, low cost, coupled with an ability to integrate with a high degree of sophistication and complexity. Reliability is the key element for a microfabricated device being used for a long period of time without any fault and errors.

4.2.1. Contamination issue. Any contaminants, such as dust particles suspended in air, may compromise the reliability of the entire system. All reliability issues concerned with microfabrication are directly and indirectly related to the clean room technology environment. The clean room is a workplace where the air quality, temperature and humidity are highly regulated in order to protect sensitive equipment from contaminations, native oxide growth, dust particles and other related harmful factors and it is crucial in case of lithography.

For photolithography, the main concerns over the various cleaning issues include the photolithography mask, photoresist and etchant used, and silicon wafer itself. The primary sources of defects are airborne contamination, such as small dust particles (invisible by naked eye), increased amount of molecular organic materials like amines that resists cleaning materials. The detection of these contaminants and their effect on yield loss is a challenge to the industry.

4.2.2. Resolution issue. The fundamental limitation in optical photolithography is the trade-off between speed and resolution [145]. Non-radiation patterning has their own challenges. For example, mechanical patterning such as nano-imprint is a form of contact lithography, facing issues of defect density, mask cost, mask damage, and wafer throughput. The throughput is an important issue in EBL, whereas the DOF is a main issue in optical lithography, and investment cost is

the major issue in x-ray lithography. The dimensions of microfabricated device will continue to shrink as the scaling enables higher speed and greater density. Lithography equipment, resist processes, and mask-making will keep changing to meet the challenges.

4.2.3. Cost issue. The high price of exposure tools has made the cost of lithography a concern and lithography costs may ultimately limit patterning capability. To meet the demands of the consumer, lithography will need to be costeffective, in addition to providing technical capability. Lithography tools are often the most expensive investment in a cleanroom. Even when they are not, the fact that lithography is required for patterning many layers in microfabrication process, while most other tools are used for only a few steps, means that a large number of lithography tools are needed for each cleanroom, resulting in high overall total costs. Wafer steppers are the most expensive pieces of equipment in the lithography tool set. Their prices have increased by an average of 17% per year since they were introduced in the late 1970s, to the point where leading-edge step-and-scan systems now cost close to \$20 M, and their prices are projected to increase in the future [113].

4.3. Issues and challenges in combined approach

Meso and micro scales are appropriately dealt with in the combined technique as examples exists in the form of lithography followed by abrasive machining and lithography followed by welding, bonding and finishing processes [104, 146]. The combined approach is not yet a formal manufacturing classification, but there are a growing number of applications especially in medical devices. A developing field of research is the flexibility of processing multiple materials in case of stereolithography 3D micro printing. A variety of materials can be employed using stereolithography and other combination of techniques, however, tackling low production rates and material strength issues are a challenge.

5. Process effectiveness guideline

A guideline can be discussed after looking at the NLBMM and LBMM issues and technical challenges with regards to the future trends. Though the two techniques have their specific zones with regards to scale and feature dimensional and shape complexity, there is a potential for combined approach as well where any of the two techniques can work as the baseline technique with the other one as a finishing process. Figure 5 highlights an overlapping zone where the three approaches can overlap. The zone reflects the meso scale with 3D features, where NLBMM can be used with variety of materials, however, LBMM techniques are being used to make very slender, irregular 3D shapes, hollow or freestanding structures.

With the advent in IoT based technologies, manufacturing of low-cost sensors and MEMS are further pushing the demand for large scale production. This will increase in micro machining requirements of ceramics, piezo and other sensor



Figure 5. Overlapping zone.

	Feature Size	in ten	w mm				M	ater	Non	contouts is	colamics metals	Polym	cita					
	Photolithography (contact & proximity)			0	0	0					0	0		\bullet	\bullet		\bullet	0
	Photolithography (Projection)		0	0	0	0	\bullet	\bullet	\bullet	\bullet	0	0		\bullet		\bullet	\bullet	0
	Electron Beam	0	0	0	\bullet	\bullet	\bullet	\bullet	۲	۲	0	0		\bullet	0	0	\bullet	\bullet
LBMM	Ion Beam	0	0	0	\bullet	\bullet	\bullet	\bullet	۲	\bullet	0	0		\bullet	0	0	\bullet	\bullet
	X-ray	0	0	0	\bullet	\bullet	\bullet	\bullet	\bullet	\bullet	0	0	\bullet	\bullet	0	0	\bullet	\bullet
	Extreme UV	0	0	0	ullet	\bullet	\bullet	•	\bullet	\bullet	0	0	\bullet	\bullet	0	0	•	•
	μ milling, μ turning	0			0	0	0	•	•	•	•	•	0		0		•	•
	μ drilling	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	Õ	ŏ	ŏ	ŏ	ŏ	Õ	Ō
	μ grinding	ŏ	Ŏ	Ŏ	0	•	Ŏ	Ŏ	Ŏ	Ŏ	Ō	Ō	ŏ	ō	Ŏ	Õ	•	Õ
	μ shaping	Ō	Ō	•	Ō	0	0	\bullet	•	•	•	•	Ō	Ō	0	Õ	0	0
	μ EDM, μ WEDM	•	•	•	0	0	\bullet	\bullet			•	•	0	0	0	0	\bullet	0
NLBMM	μECM	•	•	•	0	0	\bullet	\bullet	\bullet	\bullet	•	•	0	0	0	0	ullet	0
	Laser μ machining	0	•	•	0	0	\bullet	\bullet			\bullet	\bullet		\bullet	0	ullet	ullet	0
	μ 3D printing	\bullet			0	0	0	\bullet			\bullet	\bullet	\bullet	\bullet	0	0	\bullet	ullet
	μ molding	\bullet			0	0	0	0			\bullet	\bullet	0	\bullet	0	0	0	\bullet
	μ Laser Sintering	\bullet			0	0	0	0	0	\bullet	\bullet	\bullet	\bullet	\bullet	0	0	\bullet	\bullet
Combined Approach	Stereolithography + μ LBMM process	0	0		0	0	0	0	Ο		0	0	0	\bullet	0	0	ullet	\bullet
 High Medium Low 		/	TO	un to solera	unin Toy	un I	un or	100r		/	/ P	/s	uction of the second second	Poton Pedium	te Geomes & hot Size	sound contraction	mplexity	./

Figure 6. Overall summary: process effective guideline for meso/micro manufacturing.

materials and hence, the new technologies in overlapping zone are possibly emerging. This overlapping zone can be considered as the window of opportunity in the future of micromeso scale manufacturing as meso scale assembly can employ components built through numerous processes of NLBMM, LBMM and combined approaches with materials flexibility, cost effectiveness and multi scale component integration for diverse applications.

When NLBMM techniques go beyond micro-meso domain, the challenges increase with further reduction in size. In contrary, for modern day LBMM processes, the normal feature size has reduced in the range of 10–50 nm. Figure 6 reveals an overall guideline for the NLBMM, LBMM and combined approach processes in terms of feature size, achievable tolerances, materials and production rate. Each category is further divided into few sub-categories for detailed working like feature sizes are divided in to three ranges of micro and meso scales. Similarly, achievable tolerances are divided into six ranges from nano to micro-meter. For materials, ferrous, non-ferrous, ceramics and polymers are identified and for production rate, prototyping to mass production is categorized. A total of six LBMM, ten NLBMM and one combined approach process is tabulated. There are three categories defined for low, medium and high effectiveness with the process.

The trend shows that micro NLBMM processes are more relevant in meso scale, but they are not suited in mass production. There is a mix pattern for the achievable geometrical complexity in micro meso scale features for both NLBMM and LBMM. A recent development is the ability of LBMM and stereolithography processes combined to make functional components at micro meso scale has created an edge and found as a fully developed combined approach. Sputtering and CVD are used to deposit metals and non-metals materials onto SLA built polymer substrate to make them functional by finishing through chemical etching. On NLBMM side, micro 3D printing is employed recently for development of functional components and manufacturers are looking for mass production of micro 3D printed functional parts as the new way forward. Flexible 3D printed assemblies and fabrics have the potential in textile, fashion and medical industries. Some examples of 3D printed functional assemblies are ball & socket joint, bearings and functional hinges and chains. Stereolithography based 3D printing is the most advanced process for detailed concept models with better finish for functional and non-functional parts.

6. Conclusion

The study in this paper by comparing lithography versus NLBMM reveals different manufacturing options for a given requirement. It is concluded that some of the present day NLBMM techniques are in nascent stage but have a promising future. Various 3D micro products have been attempted in NLBMM with a very high accuracy level. Although, the micro products like semi-conductor and MEMS devices have not taken considerable attention by NLBMM techniques, as these applications are widely served through LBMM based techniques. The focus of LBMM processes is more towards micro and nano scale, therefore, meso scale is still exploited by more NLBMM and stereolithography approaches. Manufacturers are employing ways to increase the production rates to cater for high demand of meso scale parts and products. The cost effectiveness of NLBMM processes for production of meso scale parts can be enhanced, if the technological development can made possible for the availability of cheaper high precision machinery.

Data availability statement

All data that support the findings of this study are included within the article (and any supplementary files).

Acknowledgments

The authors would like to acknowledge the support of KERNmicrotechnik, Germany and Boston Micro Fabrication, USA for their support in providing artifact sample figures. Certain images in this publication have been obtained by the author(s) from the Wikipedia/Wikimedia website, where they were made available under a Creative Commons licence or stated to be in the public domain. Please see individual figure captions in this publication for details. To the extent that the law allows, IOP Publishing disclaim any liability that any person may suffer as a result of accessing, using or forwarding the image(s). Any reuse rights should be checked and permission should be sought if necessary from Wikipedia/Wikimedia and/or the copyright owner (as appropriate) before using or forwarding the image(s).

ORCID iDs

Azfar Khalid b https://orcid.org/0000-0001-5270-6599 Yang Wei b https://orcid.org/0000-0001-6195-8595 Waqas Akbar Lughmani b https://orcid.org/0000-0003-2989-1559

References

- Kawahara N, Suto T, Hirano T, Ishikawa Y, Kitahara T, Ooyama N and Ataka T 1997 Microfactories; new applications of micromachine technology to the manufacture of small products *Microsyst. Technol.* 3 37–41
- [2] Okazaki Y, Mishima N and Ashida K 2004 Microfactory-concept, history and developments J. Manuf. Sci. Eng. 126 837–44
- [3] Ashida K, Mishima N, Maekawa H, Tanikawa T, Kaneko K and Tanaka M 2000 Development of desktop machining microfactory -trial production of miniature machine products *Proc. Japan-USA Symp. on Flexible Automation* pp 175–8
- [4] Khalid A and Mekid S 2006 Design of precision desktop machine tools for meso-machining 2nd I* PROMS Virtual International Conference 3–14 July 2006 Proc. 2nd Int. Conf. on Intelligent Production Machines and Systems pp 165–70

- [5] Uriarte L, Herrero A, Zatarain M, Santiso G, de Lacalle L N L, Lamikiz A and Albizuri J 2007 Error budget and stiffness chain assessment in a micromilling machine equipped with tools less than 0.3 mm in diameter *Precis. Eng.* 31 1–12
- [6] Alting L, Kimura F, Hansen H N and Bissacco G 2003 Micro engineering Ann. CIRP 52 635–57
- [7] Kornel F E *et al* 2005 WTEC panel report on international assessment of research and development in micromanufacturing (World Technology Evaluation Center (WTEC), Inc.)
- [8] Jahan M P, Rahman M, Wong Y S and Fuhua L 2010 On-machine fabrication of high-aspect-ratio micro electrodes and application in vibration-assisted micro-electrodischarge drilling of tungsten carbide *Proc. Inst. Mech. Eng.* B 224 795–814
- [9] Chang-Sheng L, Yunn-Shiuan L, Yi-Ting C and Yunn-Cheng L 2010 Fabrication of micro ball joint by using micro EDM and electroforming *Microelectron. Eng.* 87 1475–8
- [10] Liu K, Lauwers B and Reynaerts D 2010 Process capabilities of micro-EDM and its applications Int. J. Adv. Manuf. Technol. 47 11–19
- [11] Byrne B, Dornfeld G and Denkena D 2003 Advancing cutting technology CIRP Ann. 52 483–507
- [12] Dornfeld D, Min S and Takeuchi Y 2006 Recent advances in mechanical micromachining CIRP Ann. 55 745–68
- [13] (Available at: http://fanuc.co.jp/en/product/robonano/ index.html) (Accessed 21 August 2021)
- [14] Bhattacharyya B 2015 Electrochemical Micromachining for Nanofabrication, MEMS and Nanotechnology (Kolkata Elsevier)
- [15] Sidorkin V, van Run A, van Langen-suurling A, Grigorescu A and van der Drift E 2008 Towards 2–10 nm electron-beam lithography: a quantitative approach *Microelectron. Eng.* 85 805–9
- [16] Ito T and Okazaki S 2000 Pushing the limits of lithography Nature 406 1027–31
- [17] Luong V 2018 Presentation EUV lithography coming to your local IC manufacturer! SoonTM Arenberg Youngster Seminar (Leuven)
- [18] Credgington D, Fenwick O, Charas A, Morgado J, Suhling K and Cacialli F 2010 High-resolution scanning near-field optical lithography of conjugated polymers Adv. Funct. Mater. 20 2842–7
- [19] Nakasugi T *et al* 2018 Half pitch 14 nm direct pattering with nanoimprint lithography *IEEE Int. Electron Devices Meeting (IEDM) (San Francisco, CA)* pp 11.7.1–4
- [20] Zhang Y, Luo J, Xiong Z, Liu H, Wang L, Gu Y, Lu Z, Li J and Huang J 2019 User-defined microstructures array fabricated by DMD based multistep lithography with dose modulation *Opt. Express* 27 31956
- [21] Kirchner R and Taniguchi J 2019 Toward full three-dimensional (3D) high volume fabrication Adv. Opt. Technol. 8 171–3
- [22] Azizur Rahman M, Rahman M, Senthil Kumar A and Lim H S 2005 CNC microturning: an application to miniaturization Int. J. Mach. Tools Manuf. 45 631–9
- [23] Takeuchi Y, Yonekura H and Sawada K 2003 Creation of 3D tiny statue by 5 axis control ultraprecision machining *Comput. Aided Des.* 35 403–9
- [24] Khalid A and Khan Z H 2014 Multi-objective optimization for error compensation in intelligent micro-factory CPS *Computational Intelligence for Decision Support in Cyber-Physical Systems* (Berlin: Springer) pp 67–103
- [25] Rowe W B 2018 Towards high productivity in precision grinding *Inventions* 3 1–16
- [26] Wu Y-Y, Huang T-W and Sheu D-Y 2020 Desktop micro-EDM system for high-aspect ratio micro-hole

drilling in tungsten cemented carbide by cut-side micro-tool *Micromachines* **11** 675

- [27] Burkhardt F, Schirmeister C G, Wesemann C, Nutini M, Pieralli S, Licht E H, Metzger M, Wenz F, Mülhaupt R and Spies B C 2020 Pandemic-driven development of a medical-grade, economic and decentralized applicable polyolefin filament for additive fused filament fabrication *Molecules* 25 5929
- [28] O'Toole L, Kang C W and Fang F Z 2021 Precision micro-milling process: state of the art *Adv. Manuf.* 9 173–205
- [29] Mamedov A 2021 Micro milling process modeling: a review Manuf. Rev. 8
- [30] Rahman M A, Rahman M, Mia M, Asad A B M A and Fardin A 2019 Manufacturing of Al alloy microrods by micro cutting in a micromachining center *Micromachines* 10 831
- [31] Brinksmeier E and Preuss W 2012 Micro-machining *Phil. Trans. R. Soc.* A **370** 3973–92
- [32] Bisaria H and Shandilya P 2015 Machining of metal matrix composites by EDM and its variants: a review DAAAM International Scientific Book ed B Katalinic (Vienna) pp 267–82
- [33] Groover M P 2010 Fundamentals of Modern Manufacturing: Materials, Processes, and Systems (USA: Wiley)
 [34] File:Wire erosion.png (available at: https://commons.
- wikimedia.org/wiki/File:Wire_erosion.png) (Accessed 23 March 2022)
- [35] Prakash S and Kumar S 2017 *Microchannel Fabrication via Direct Laser Writing* (Amsterdam: Elsevier)
- [36] File:LaserCutter.svg (available at: https://commons. wikimedia.org/wiki/File:LaserCutter.svg) (Accessed 23 March 2022)
- [37] Ngo T D, Kashani A, Imbalzano G, Nguyen K T and Hui D 2018 Additive manufacturing (3D printing): a review of materials, methods, applications and challenges *Composites* B 143 172–96
- [38] Scopigno R, Cignoni P, Pietroni N, Callieri M and Dellepiane M 2017 Digital fabrication techniques for cultural heritage: a survey *Comput. Graph. Forum* 36 6–21
- [39] (Available at: www.kern-microtechnik.com) (Accessed 21 August 2021)
- [40] Galloway L 2021 3D integrated microelectronic subsystems and additive manufacturing (Boston Micro Fabrication) (available at: https://bmf3d.com/resource/3d-integratedmicroelectronic-subsystems-and-additivemanufacturing/) (Accessed 9 December 2021)
- [41] Jonušauskas L, Gailevičius D, Rekštytė S, Baldacchini T, Juodkazis S and Malinauskas M 2019 Mesoscale laser 3D printing Opt. Express 27 15205–21
- [42] (Available at: www.nanowave.co.jp) (Accessed 21 August 2021)
- [43] (Available at: www.mikrotools.com) (Accessed 15 December 2021)
- [44] (Available at: www.agie.com) (Accessed 21 August 2021)
- [45] KERN Pyramid Nano (available at: https://swissinstruments. com/my_products/pyramid-nano-5-axis-cnc/) (Accessed 20 July 2021)
- [46] Rizvi N H and Apte P 2002 Developments in laser micro-machining techniques J. Mater. Process. Technol. 127 206–10
- [47] Mishra S and Yadava V 2015 Laser beam micromachining (LBMM)—a review Opt. Lasers Eng. 73 89–122
- [48] Ma X and Schuster R 2011 Locally enhanced cathodoluminescence of electrochemically fabricated gold nanostructures J. Electroanal. Chem. 662 12–16
- [49] Leese R J and Ivanov A 2016 Electrochemical micromachining: an introduction Adv. Mech. Eng. 8 1–13

- [50] Huo D, Chen W, Teng X, Lin C and Yang K 2017 Modeling the influence of tool deflection on cutting force and surface generation in micro-milling *Micromachines* 8 188
- [51] Okazaki Y and Kitahara T 2001 Development and Evaluation of a micro-lathe equipped with numerical control J. Japan Soc. Precis. Eng. 67 1878–83
- [52] Ogedengbe T I 2010 A contribution to the design and operation of a micro milling machine *PhD Thesis* University of Manchester, UK
- [53] Nguyen N, Wereley S T and Shaegh S A M 2002 Fundamentals and Applications of Microfluidics 3rd edn (Norwood, MA: Artech House)
- [54] Guruparan G K, Sathish M, Subramaniam N S and Kumar T S 2006 Design and fabrication of micro-channels for MEMS applications J. Synth. React. Inorg. Met-Org. Nano-Met. Chem. 36 185–91
- [55] Liu H T 1998 Near-net shaping of optical surfaces with abrasive suspension jets 14th Int. Conf. on Jetting Technology (Brugge) pp 285–94
- [56] Cheng J Y, Wei C W, Hsu K H and Young T H 2004 Direct-write laser micromachining and universal surface modification of PMMA for device development *Sens. Actuators* B 99 186–96
- [57] Snakenborg D, Klank H and Kutter J P 2004 Microstructure fabrication with a CO₂ laser system J. Micromech. Microeng. 14 182–9
- [58] Harvey E C, Rumsby P T, Gower M C and Remnant J L 1995 Microstructuring by excimer laser Micromach. Microfabr. Process. Technol. 2639
- [59] Pantelis D and Psyllaki P 1996 Excimer laser micromachining of CMSX2 and TA6V alloys *Mater*. *Manuf. Process.* 11 273–82
- [60] Heckele M and Schomburg W K 2004 Review on micro molding of thermoplastic polymers J. Micromech. Microeng, 14 R1
- [61] Jonušauskas L, Juodkazis S and Malinauskas M 2018 Optical 3D printing: bridging the gaps in the mesoscale J. Opt. 20
- [62] Kunwar P, Xiong Z, Zhu Y, Li H, Filip A and Soman P 2019 Hybrid laser printing of 3D, multiscale, multimaterial hydrogel structures Adv. Opt. Mater. 7 1900656
- [63] Wilkinson N J, Smith M A A, Kay R W and Harris R A 2019 A review of aerosol jet printing—a non-traditional hybrid process for micro-manufacturing *Int. J. Adv. Manuf. Technol.* **105** 4599–619
- [64] Ru C, Luo J, Xie S and Sun Y 2014 A review of non-contact micro- and nano-printing technologies J. Micromech. Microeng. 24 053001
- [65] Vyatskikh A, Delalande S, Kudo A, Zhang X, Portela C M and Greer J R 2018 Additive manufacturing of 3D nano-architected metals *Nat. Commun.* 9 593
- [66] Wang X, Jiang M, Zhou Z, Gou J and Hui D 2017 3D printing of polymer matrix composites: a review and prospective *Composities* B 110 442–58
- [67] Kunwar P, Jannini A V S, Xiong Z, Ransbottom M J, Perkins J S, Henderson J H, Hasenwinkel J M and Soman P 2020 High-resolution 3D printing of stretchable hydrogel structures using optical projection lithography ACS Appl. Mater. Interfaces 12 1640–9
- [68] Beeby S et al 2004 MEMS Mechanical Sensors (Norwood, MA: Artech House)
- [69] Mullen E and Morris M A 2021 Green nanofabrication opportunities in the semiconductor industry: a life cycle perspective *Nanomaterials* 11 1085
- [70] Maluf N and Williams K 2004 An Introduction to Microelecomechanical Systems Engineering 2nd edn (Artech House Inc.)
- [71] Karim W, Tschupp S A, Oezaslan M, Schmidt T J, Gobrecht J, Van Bokhoven J A and Ekinci Y 2015

High-resolution and large-area nanoparticle arrays using EUV interference lithography *Nanoscale* 7 7386–93

- [72] Joshi-Imre A and Bauerdick S 2014 Direct-write ion beam lithography J. Nanotechnol. 2014 170415
- [73] Maldonado J R and Peckerar M 2016 X-ray lithography: some history, current status and future prospects *Microelectron. Eng.* 161 87–93
- [74] Rath T, Padeste C, Vockenhuber M, Fradler C, Edler M, Reichmann A, Letofsky-Papst I, Hofer F, Ekinci Y and Griesser T 2013 Direct extreme UV-lithographic conversion of metal xanthates into nanostructured metal sulfide layers for hybrid photovoltaics *J. Mater. Chem.* A 1 11135–40
- [75] Okazaki S 1991 Resolution limits of optical lithography J. Vac. Sci. Technol. B 9 2829–33
- [76] Nakayama Y, Okazaki S and Saitou N 1990 Electron-beam cell projection lithography: a new high throughput electron direct writing technology using a specially tailored Si aperture J. Vac. Sci. Technol. B 8 1836–40
- [77] Harriott L R 2001 Limits of lithography *Proc. IEEE* 89 366–74
- [78] Cui Z 2016 Nanofabrication: Principles, Capabilities and Limits 2nd edn (Berlin: Springer)
- [79] Colson P, Henrist C and Cloots R 2013 Nanosphere lithography: a powerful method for the controlled manufacturing of nanomaterials J. Nanomater. 2013 948510
- [80] Yang X M, Peters R D, Kim T K, Nealey P F, Brandow S L, Chen M-S, Shirey L M and Dressick W J 2001 Proximity x-ray lithography using self-assembled alkylsiloxane films: resolution and pattern transfer *Langmuir* 17 228–33
- [81] Guckel H 1998 High-aspect-ratio micromachining via deep x-ray lithography *Proc. IEEE* **86** 1586–93
- [82] Chen Y 2015 Nanofabrication by electron beam lithography and its applications: a review *Microelectron. Eng.* 135 57–72
- [83] Luo C, Li Y and Susumu S 2012 Fabrication of high aspect ratio subwavelength gratings based on x-ray lithography and electron beam lithography *Opt. Laser Technol.* 44 1649–53
- [84] Pret A V, Poliakov P, Gronheid R, Blomme P, Miranda Corbalan M, Dehaene W, Verkest D, Van Houdt J and Bianchi D 2012 Linking EUV lithography line edge roughness and 16 nm NAND memory performance *Microelectron. Eng.* 98 24–28
- [85] Wu B and Kumar A 2007 Extreme ultraviolet lithography: a review J. Vac. Sci. Technol. B 25 1743
- [86] Delachat F, Drogoff B L, Constancias C, Delprat S, Gautier E and Chaker M 2016 Fabrication of high aspect ratio tungsten nanostructures on ultrathin c-Si membranes for extreme UV applications *Nanotechnology* 27025304
- [87] Hayes G R, Frecker M I and Adair J H 2011 Fabrication of compliant mechanisms on the mesoscale *Mech. Sci.* 2 129–37
- [88] Engstrom D S, Porter B, Pacios M and Bhaskaran H 2014 Additive nanomanufacturing—a review J. Mater. Res. 29 1792–816
- [89] Takahata K, Shibaike N and Guckel H 2000 High-aspect-ratio WC–Co microstructure produced by the combination of LIGA and micro-EDM *Microsyst. Technol.* 6 175–8
- [90] Giannitsis A T 2011 Microfabrication of biomedical lab-on-chip devices: a review *Est. J. Eng.* **17** 109–39
- [91] Meijer J 2004 Laser beam machining (LBM) state of the art and new opportunities *J. Mater. Process. Technol.* 149 2–17
- [92] Bilal A, Jahan M P, Talamona D and Perveen A 2018 Electro-discharge machining of ceramics: a review *Micromachines* 10 1–41

- [93] Lal A 1998 Silicon-based ultrasonic surgical actuators Proc. 20th Annual Int. Conf. IEEE Engineering in Medicine and Biology Society vol 20 pp 2785–90
- [94] Petersen K E 1982 Silicon as a mechanical material Proc. IEEE 70 420–57
- [95] Pinto E, Faustino V, Rodrigues R O, Pinho D, Garcia V, Miranda J M and Lima R 2015 A rapid and low-cost nonlithographic method to fabricate biomedical microdevices for blood flow analysis *Micromachines* 6 121–35
- [96] Vinayakumar K B, Kulkarni P G, Nayak M M, Dinesh N S, Hegde G M, Ramachandra S G and Rajanna K 2016 A hollow stainless steel microneedle array to deliver insulin to a diabetic rat J. Micromech. Microeng. 26 065013
- [97] Ali Z, Türeyen E B, Karpat Y and Çakmakci M 2016 Fabrication of polymer micro needles for transdermal drug delivery system using DLP based projection stereo-lithography *Proc. CIRP* 42 87–90
- [98] Indermun S, Luttge R, Choonara Y E, Kumar P, du Toit L C, Modi G and Pillay V 2014 Current advances in the fabrication of microneedles for transdermal delivery J. *Control. Release* 185 130–8
- [99] Chang Y and Huang H 2014 Nano-scale tip fabricated by electro-chemical machining for nano lithography 9th IEEE Int. Conf. on Nano/Micro Engineered and Molecular Systems, IEEE-NEMS 2014 pp 126–9
- [100] Chia H N and Wu B M 2015 Recent advances in 3D printing of biomaterials *J. Biol. Eng.* **9**
- [101] Luan B 2007 Process for chemical etching of parts fabricated by stereolithography US 2007/0108664 A1
- [102] Luan B, Yeung M, Wells W and Liu X 2000 Chemical surface preparation for metallization of stereolithography polymers *Appl. Surf. Sci.* 156 26–38
- [103] Han F, Jiang J and Yu D 2007 Influence of machining parameters on surface roughness in finish cut of WEDM *Int. J. Adv. Manuf. Technol.* 34 538–46
- [104] Chowdhury D F H and Lughmani W A 2017 Microneedle device Patent Application Number: US20190022365A1
- [105] Dixit N K, Srivastava R and Narain R 2019 Improving surface roughness of the 3D printed part using electroless plating *Proc. Inst. Mech. Eng.* L 233 942–54
- [106] Grepstad J O, Greve M M, Reisinger T and Holst B 2013 Nanostructuring of free standing, dielectric membranes using electron-beam lithography J. Vac. Sci. Technol. B 31 06F402
- [107] Xiong Z, Kunwar P and Soman P 2021 Hydrogel-based diffractive optical elements (hDOEs) using rapid digital photopatterning Adv. Opt. Mater. 9 2001217
- [108] Benavides G L, Adams D P and Yang P 2001 Meso-machining capabilities (https://doi.org/10.2172/ 782720)
- [109] Mekid S 2008 Introduction to Precision Machine Design and Error Assessment 1st edn (Boca Raton, FL: CRC Press)
- [110] Madou M J 2011 Fundamentals of Microfabrication and Nanotechnology, Volume 2, Manufacturing Techniques for Microfabrication and Nanotechnology 3rd edn (Boca Raton, FL: CRC Press)
- [111] Macdonald N P, Cabot J M, Smejkal P, Guijt R M, Paull B and Breadmore M C 2017 Comparing microfluidic performance of three-dimensional (3D) printing platforms *Anal. Chem.* 89 3858–66
- [112] Schmidleithner C and Kalaskar D M 2018 Stereolithography in 3D printing *IntechOpen* (https://doi.org/10.5772/ intechopen.78147)
- [113] Levinson H J 2005 Lithography Costs in Principles of Lithography 2nd edn (SPIE) pp 355–74
- [114] Hazelton A J, Wüest A, Hughes G, Litt L C and Goodwin F 2008 Cost of ownership for future lithography technologies *Proc. SPIE* 7140 71401Q

- [115] Moceri M 2020 How to accurately price for stereolithography (SLA) 3D printing projects (available at: https://3dprintingindustry.com/news/how-to-accuratelyprice-for-stereolithography-sla-3d-printing projects171977/) (Accessed 20 June 2021)
- [116] Mourtzis D, Vlachou E, Milas N and Dimitrakopoulos G 2016 Energy consumption estimation for machining processes based on real-time shop floor monitoring via wireless sensor networks *Proc. CIRP* 57 637–42
- [117] Wang Q, Yuan G H, Kiang K S, Sun K, Gholipour B, Rogers E T F, Huang K, Ang S S, Zheludev N I and Teng J H 2017 Reconfigurable phase-change photomask for grayscale photolithography *Appl. Phys. Lett.* 110 201110
- [118] Choi J W, Kim H C and Wicker R 2011 Multi-material stereolithography J. Mater. Process. Technol. 211 318–28
- [119] Rajabasadi F, Schwarz L, Medina-Sánchez M and Schmidt O G 2021 3D and 4D lithography of untethered microrobots *Prog. Mater. Sci.* 120 100808
- [120] Yang C, Boorugu M, Dopp A, Ren J, Martin R, Han D, Choi W and Lee H 2019 4D printing reconfigurable, deployable and mechanically tunable metamaterials *Mater. Horiz.* 6 1244–50
- [121] Chavoshi S Z, Goel S and Morantz P 2017 Current trends and future of sequential micro-machining processes on a single machine tool *Mater. Des.* 127 37–53
- [122] Georgi O, Rentzsch H and Blau P 2018 Miniaturized parallel kinematic machine tool for the machining of small workpieces in euspen's 18th Int. Conf. & Exhibition (Venice, IT)
- [123] Islam S O, Khan L A, Khalid A and Lughmani W A 2019 A smart microfactory design: an integrated approach *Functional Reverse Engineering of Machine Tools* 1st edn (Boca Raton, FL: CRC Press)
- [124] Zhao G, Deng Y, Xiao W and Liu Y 2017 Micro machine tool oriented optimum design of 3-RPS parallel mechanism with large titling and uniform deflecting capacities J. Adv. Mech. Des. Syst. Manuf. 11–13
- [125] Axinte D et al 2018 MiRoR—miniaturized robotic systems for holistic in situ repair and maintenance works in restrained and hazardous environments IEEE/ASME Trans. Mechatronics 23 978–81
- [126] Otsuka J, Hata S, Shimokohbe A and Koshimizu S 1998 Development of ultraprecision table for ductile mode cutting J. Japan Soc. Precis. Eng. 64 546–51
- [127] Holmes M, Trumpet D and Hocken R 1995 Atomic scale precision motion control stage (the Angstrom Stage) CIRP Ann. 44 455–60
- [128] Mizumoto H, Yabuta Y, Arii S, Tazoe Y and Kami Y 2005 A picometer positioning system using active aerostatic guideway Proc. Int. Conf. on Leading Edge Manufacturing in 21st Century (Nagoya, Japan) pp 1009–14
- [129] Mizumoto H, Yabuya M, Shimizu T and Kami Y 1995 An angstrom-positioning system using a twist-roller friction drive *Precis. Eng.* 17 57–62
- [130] Qiao Y and Bu H 2000 Investigation on suction force of vacuum pumps for micro-components Vacuum 56 123-8
- [131] Mishima N 2003 Design of a miniature manufacturing system for micro fabrication Proc. 10th ISPE Int. Conf. on Concurrent Engineering (Madeira, Portugal) pp 1129–35
- [132] Clavel R 2005 High precision parallel robots for micro-factory applications 2nd Int. Colloquium (Braunschweig: Collaborative Research Centre) pp 285–96
- [133] Verettas I, Clavel R and Codourey A 2003 Microfactory: desktop cleanrooms for the production of microsystems *Proc. IEEE Int. Symp. on Assembly and Task Planning* vol 2003 pp 18–23

- [134] Codourey A and Honnegger M 2002 A centralized control system for microfactories 3rd Int. Workshop on Microfactories
- [135] Trimmer W S N 1989 Microrobots and micromechanical systems Sens. Actuators 19 267–87
- [136] Mekid S, Khalid A and Ogedengbe T 2008 Common physical problems in micromachining 6th CIRP Int. Conf. on Intelligent Computation in Manufacturing Engineering—CIRP ICME '08 (Ischia (Naples), Italy)
- [137] Wahab A, Khalid A and Nawaz R 2014 Non-contact metrology inspection system for precision micro products *Int. Conf. on Robotics and Emerging Allied Technologies in Engineering (Icreate)* (https://doi.org/10.1109/ iCREATE.2014.6828356)
- [138] Mekid S and Ryu H S 2007 Rapid vision-based dimensional precision inspection of mesoscale artefacts *Proc. Inst. Mech. Eng.* B 221 659–72
- [139] Peggs G N, Lewis A J and Oldfield S 1999 Design for a compact high-accuracy CMM CIRP Ann. 48 417–20
- [140] Jäger G, Manske E, Hausotte T and H-j B 2000 Laserinterferometrische Nanomessmaschinen, VDI

Berichte, 1530 (Sensoren und Messsysteme 2000) (Düsseldorf: VDI Verlag GmbH)

- [141] Min S, Lidde J, Raue N and Dornfeld D 2011 Acoustic emission based tool contact detection for ultra-precision machining CIRP Ann. 60 141–4
- [142] Takeuchi Y, Sawada K and Kawai T 1997 Three dimensional micromachining by means of ultraprecision milling *Proc.* 9th Int. Precision Engineering Seminar and 4th Int. Conf. on Ultraprecision in Manufacturing Engineering pp 596–9
- [143] Sasaki T, Takeuchi Y, Kawai T and Sakaida Y 2004 5-axis control ultraprecision micromachining of micro 3D body *Proc. Spring Annual Meeting of JSPE* pp 1075–6
- [144] Ogedengbe T I 2014 Tool condition monitoring on micro milling machine using current signature and radial basis function (RBF) network *Res. J. Eng. Appl. Sci.* **3** 208–15
- [145] Iwai H 2009 Roadmap for 22 nm and beyond *Microelectron*. Eng. 86 1520–8
- [146] Chowdhury D F H, Lughmani W A and Voulgaris S 2017 Device and method *Patent Application Number:* WO2017129964A1